

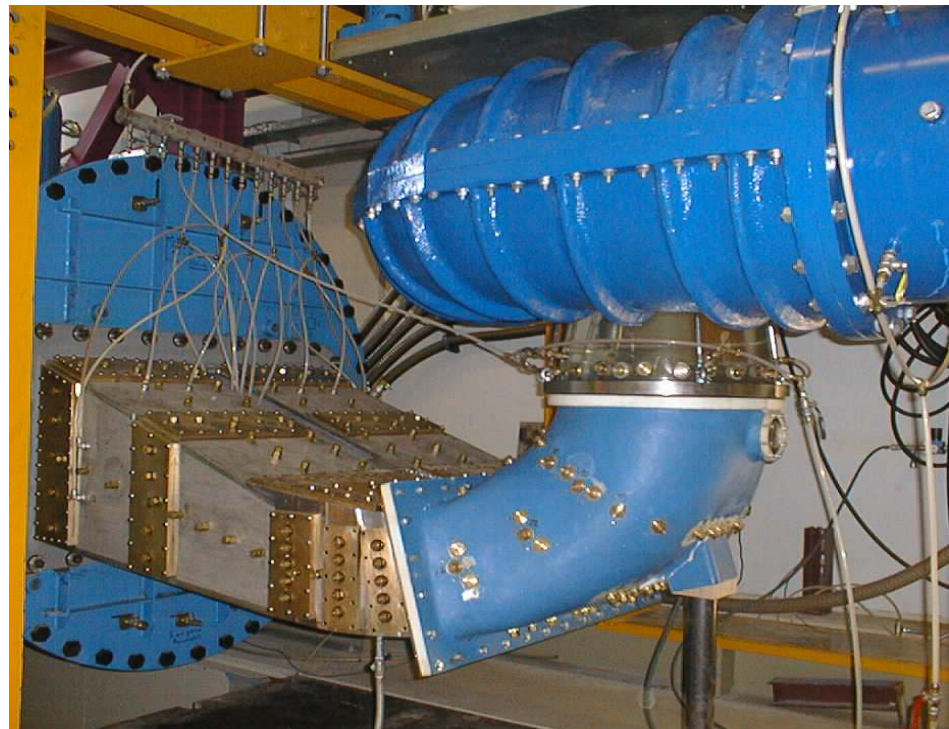
*Metode moderne pentru cercetarea in
Masini Hidraulice*



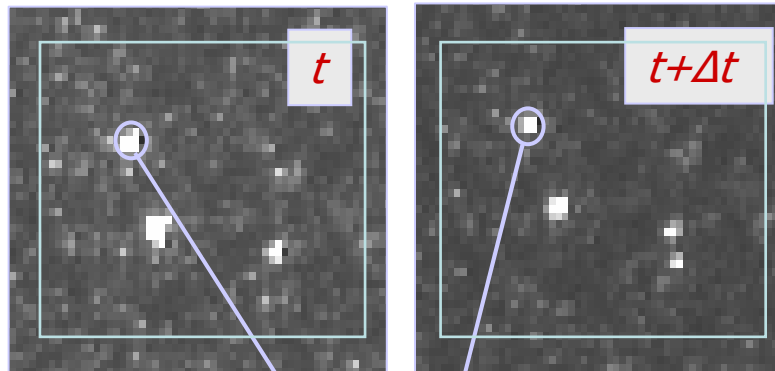
**Metode moderne pentru
cercetarea in Masini Hidraulice**



*Dr. Gabriel Dan CIOCAN
Associate Professor*

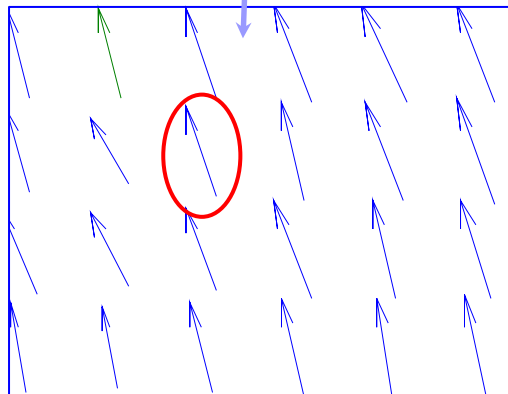


3D PIV Principle



FFT analysis

Cross-correlation



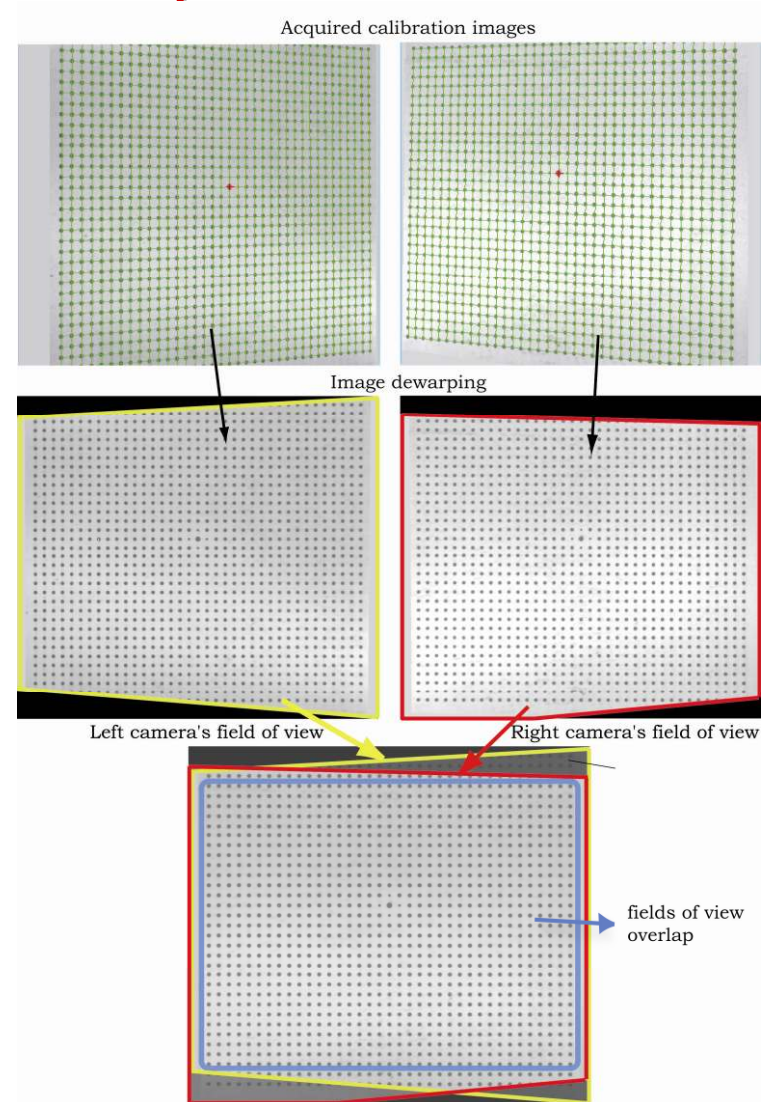
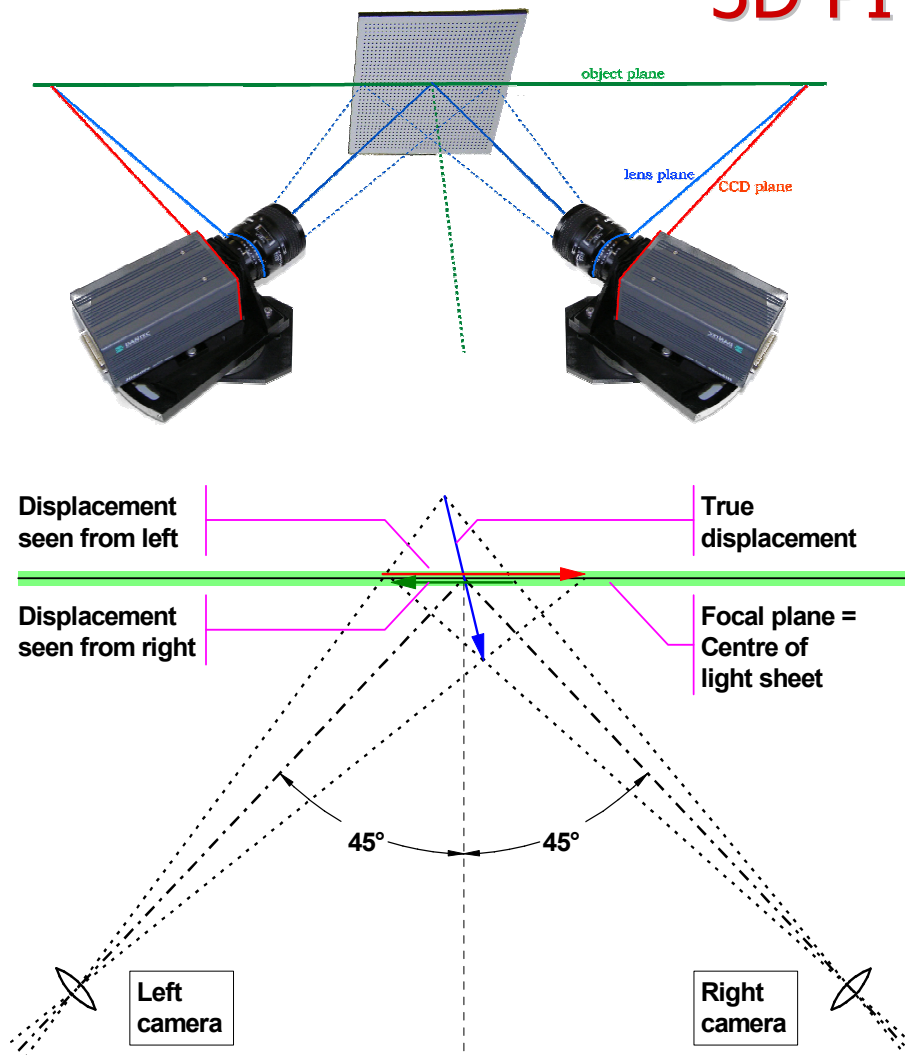
✓ *Acquisition Parameters*

- time interval
- seeding density
- energy distribution in the laser-sheet
- laser-sheet alignment

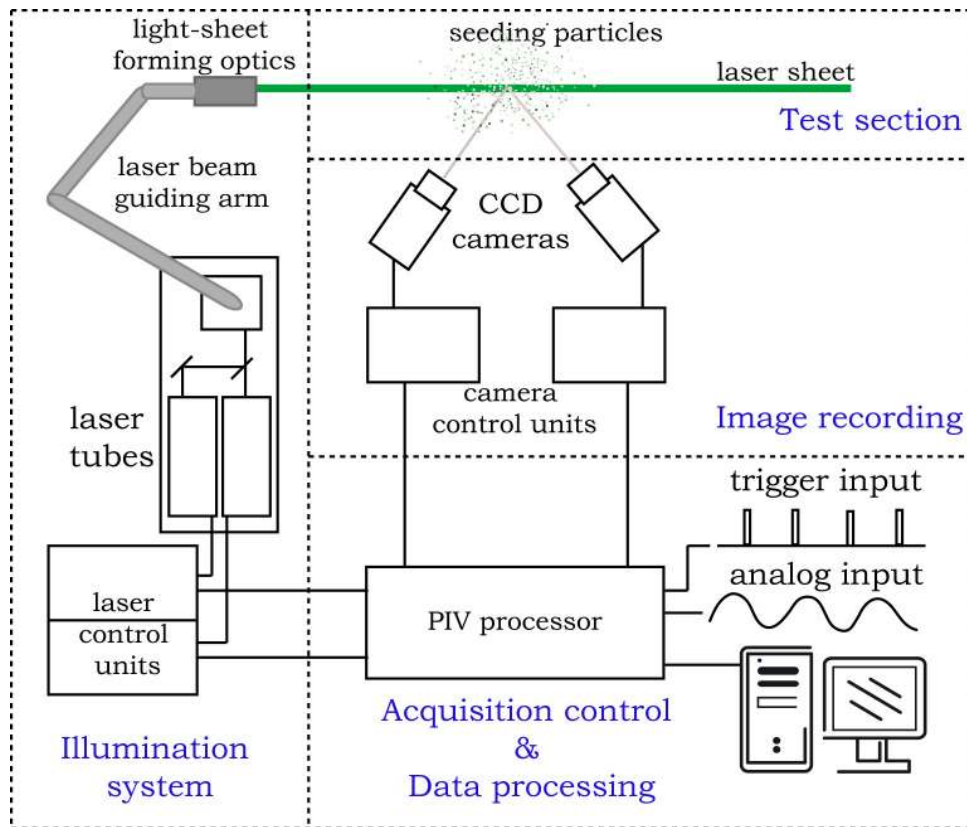
✓ *Vectors Fields Validation*

- masking
- correlation quality
- moving average interpolation

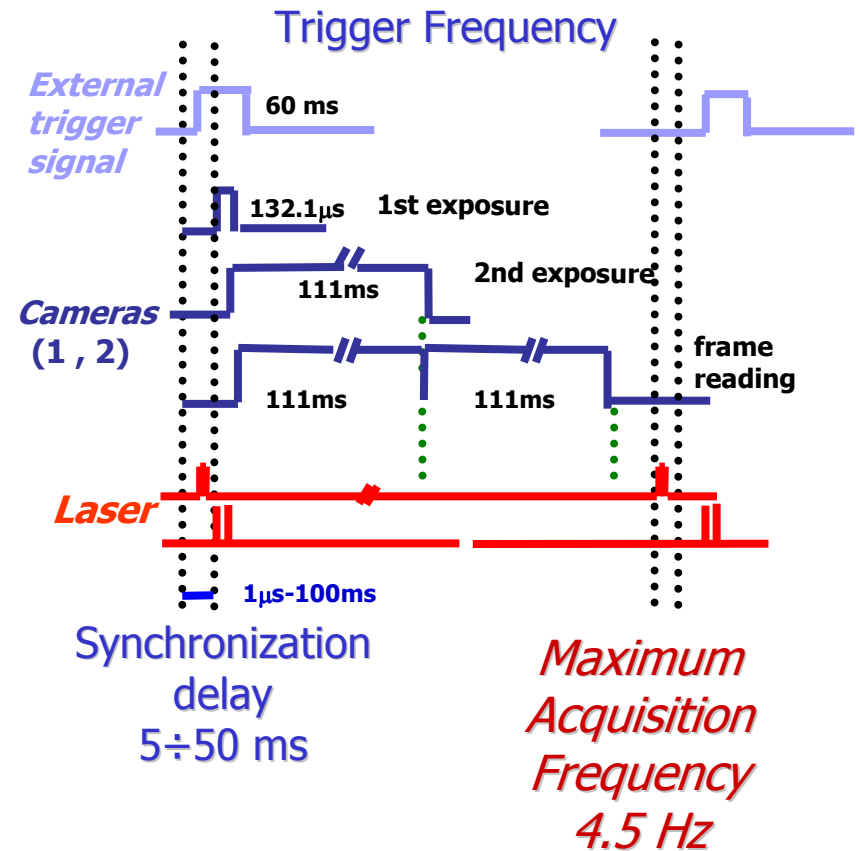
3D PIV Principle



PIV System

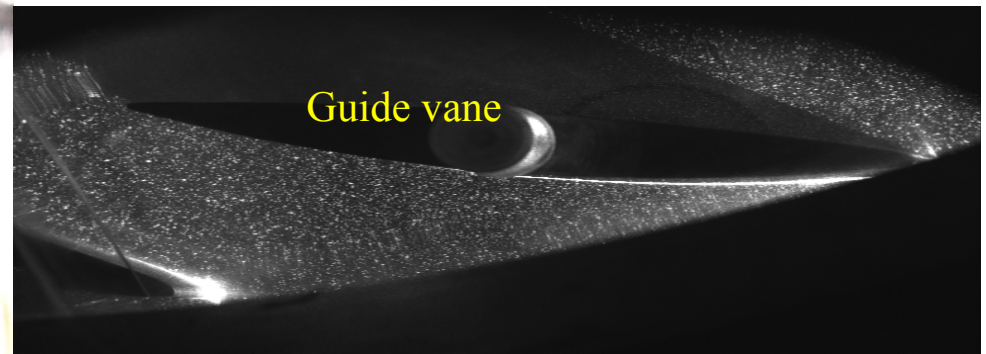
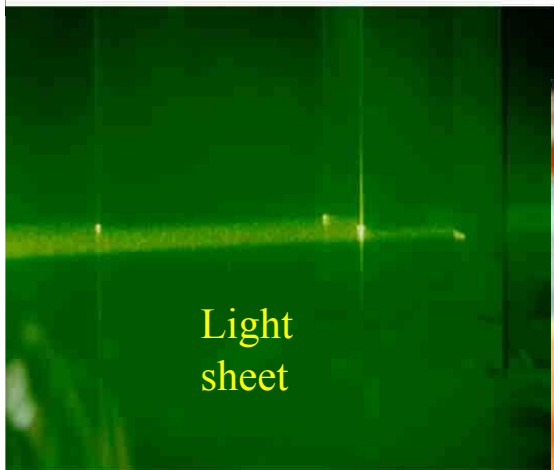
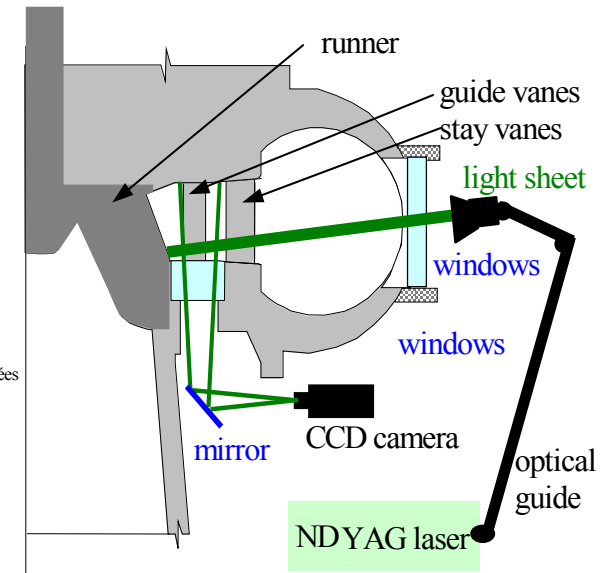
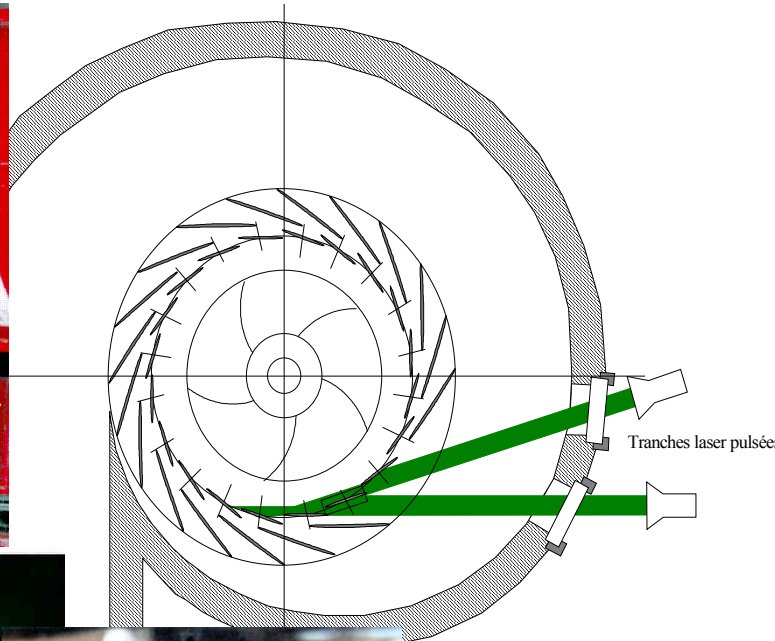
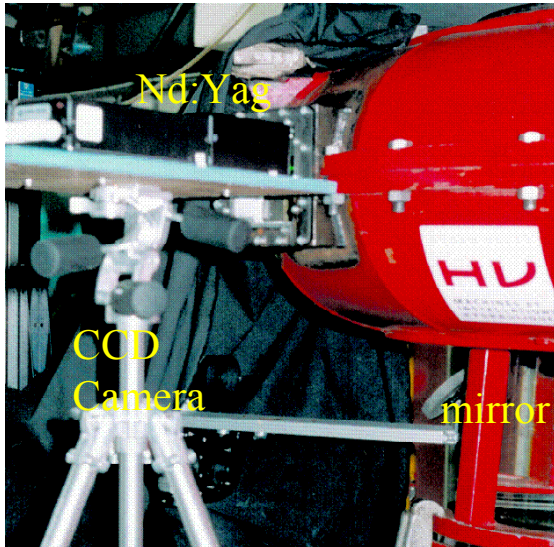


System Architecture

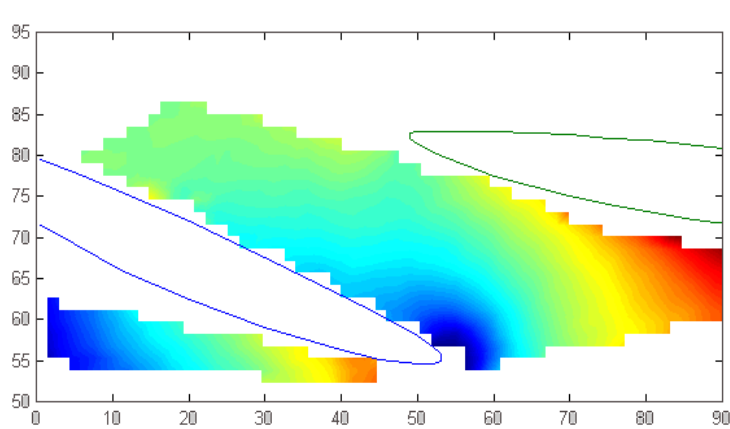


Timing Diagram

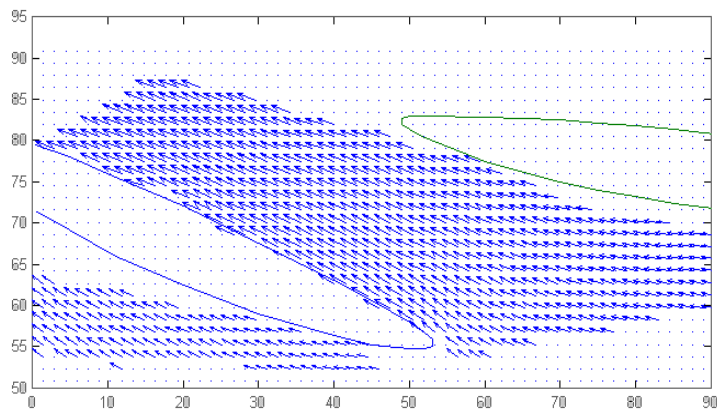
Rotor-Stator Interaction



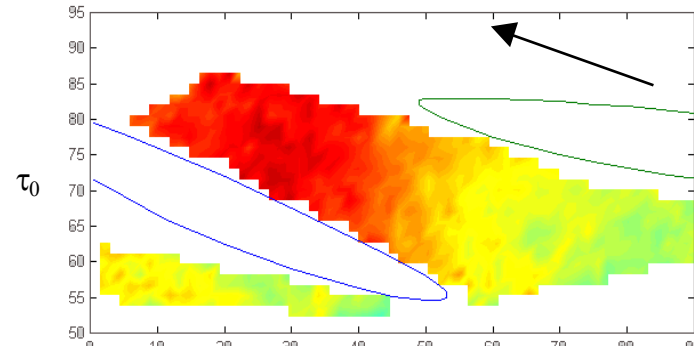
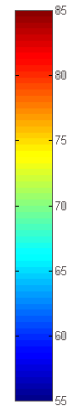
Turbine Rotor-Stator Interaction



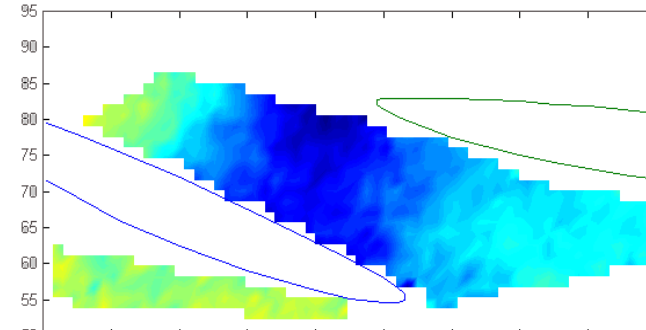
Angle of the Velocity Vector



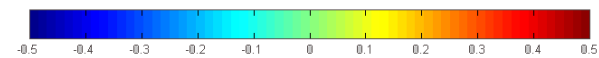
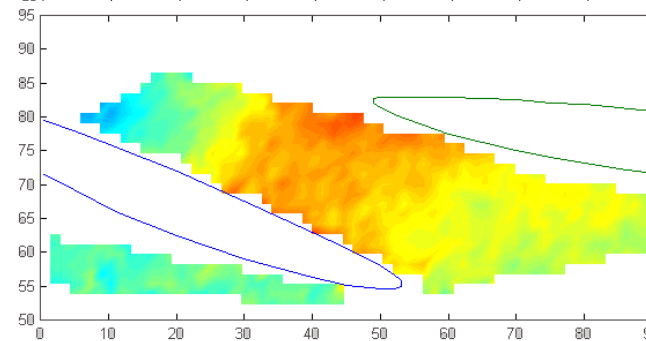
Mean Velocity Field



$\tau_0 + 28.8^\circ$

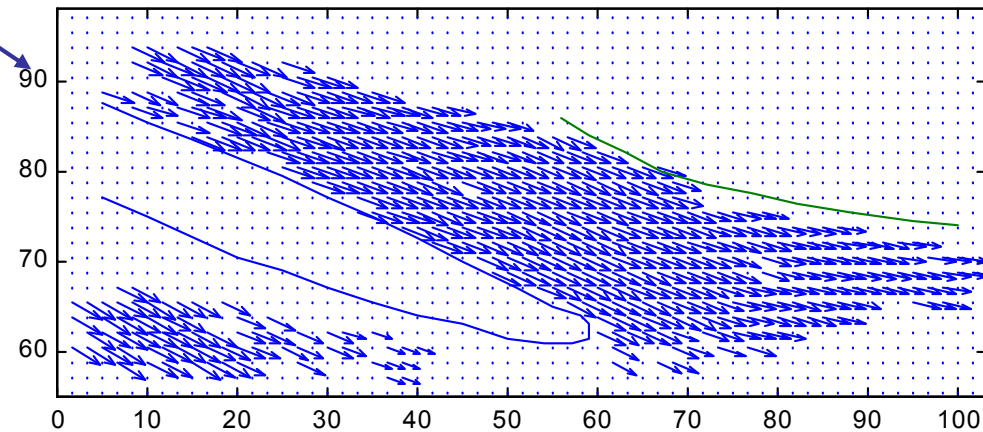
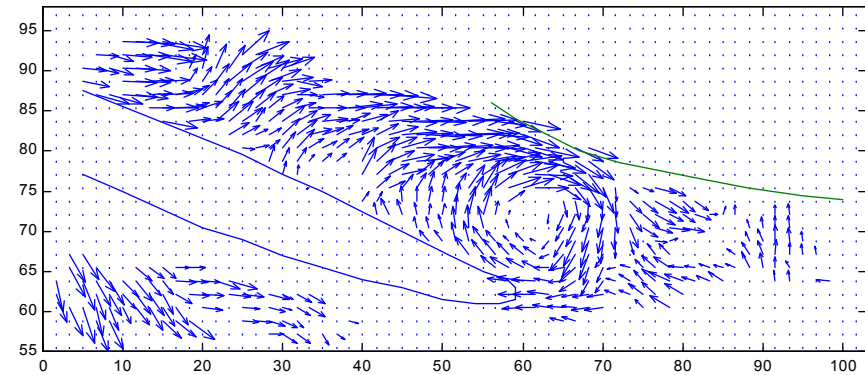
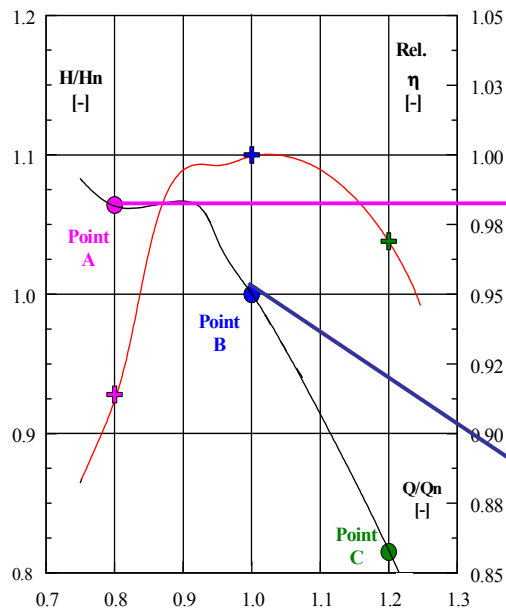


$\tau_0 + 57.6^\circ$



$\tilde{c} - \bar{c}$

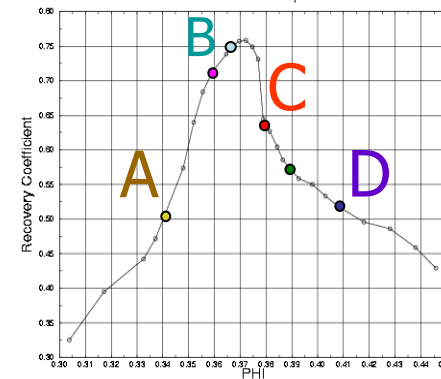
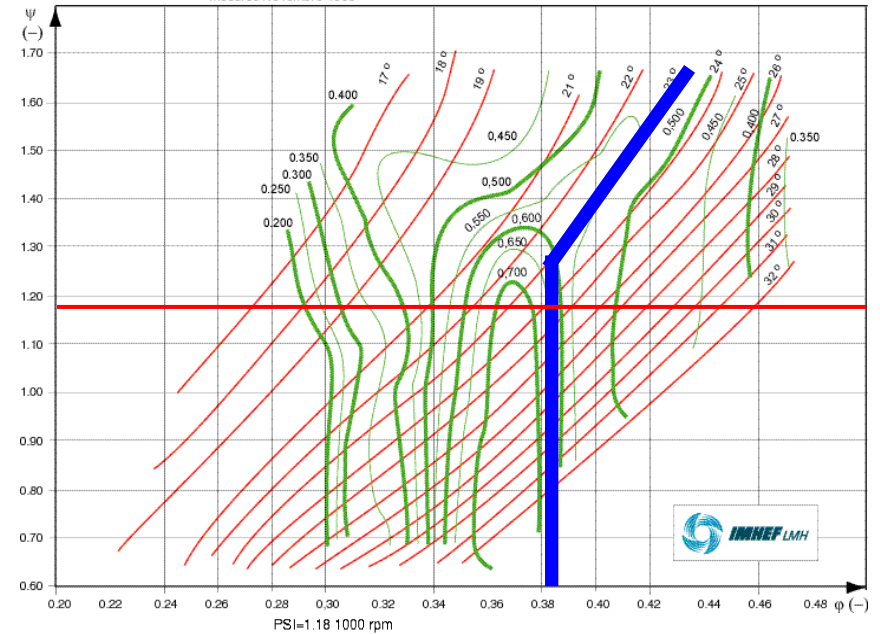
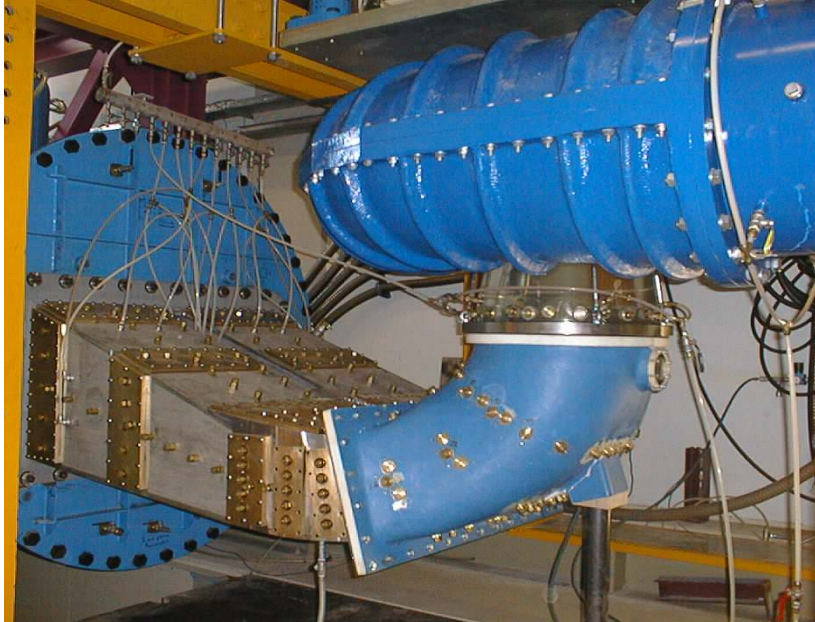
Pump Rotor-Stator Interaction



Metode moderne pentru cercetarea in Masini Hidraulice



FLINDT Project

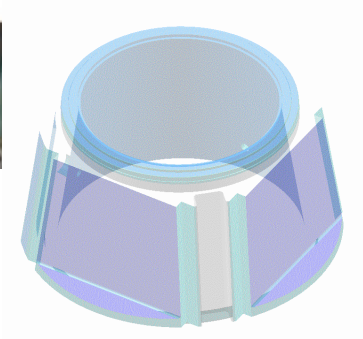
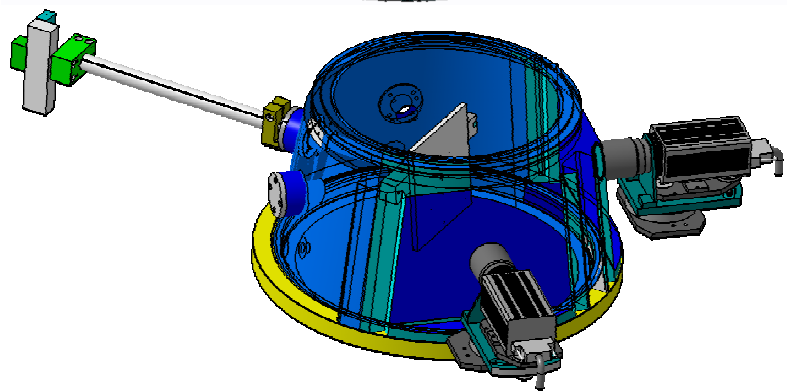
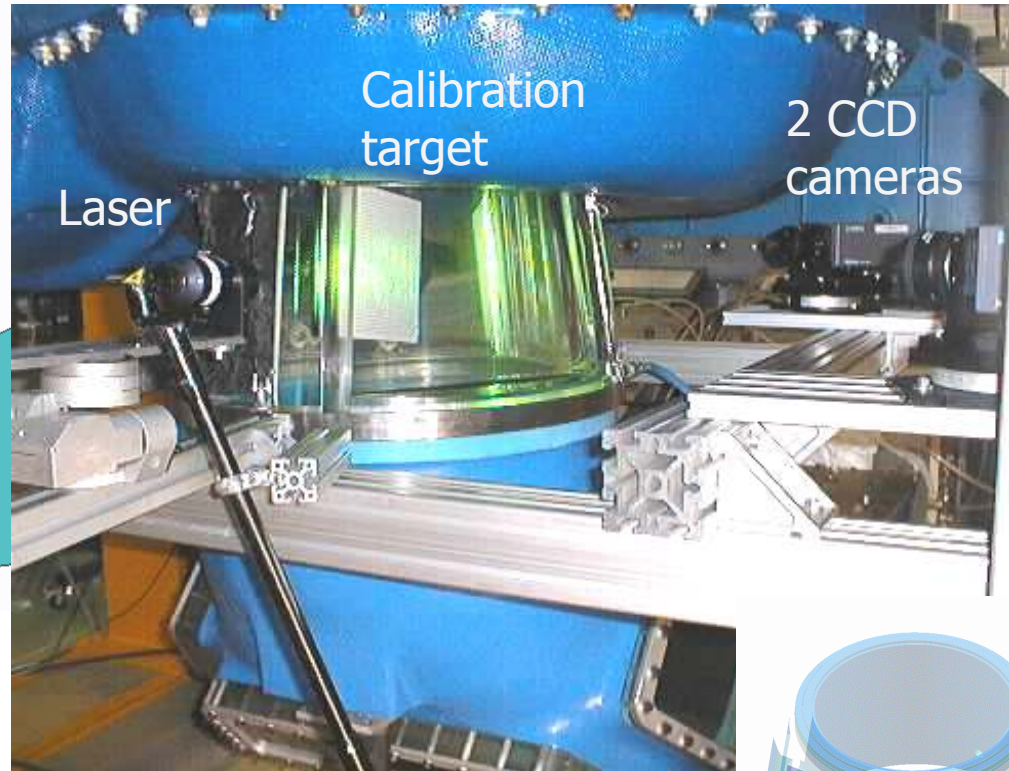
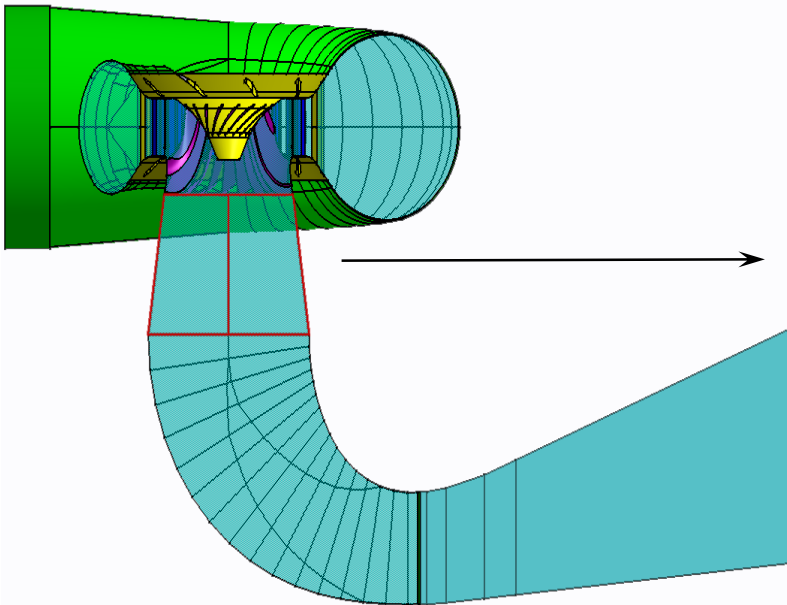


$$\chi = \frac{\frac{1}{\rho} \Delta p_{asp}}{\frac{1}{2} \left(\frac{Q}{A_{ref}} \right)^2}$$

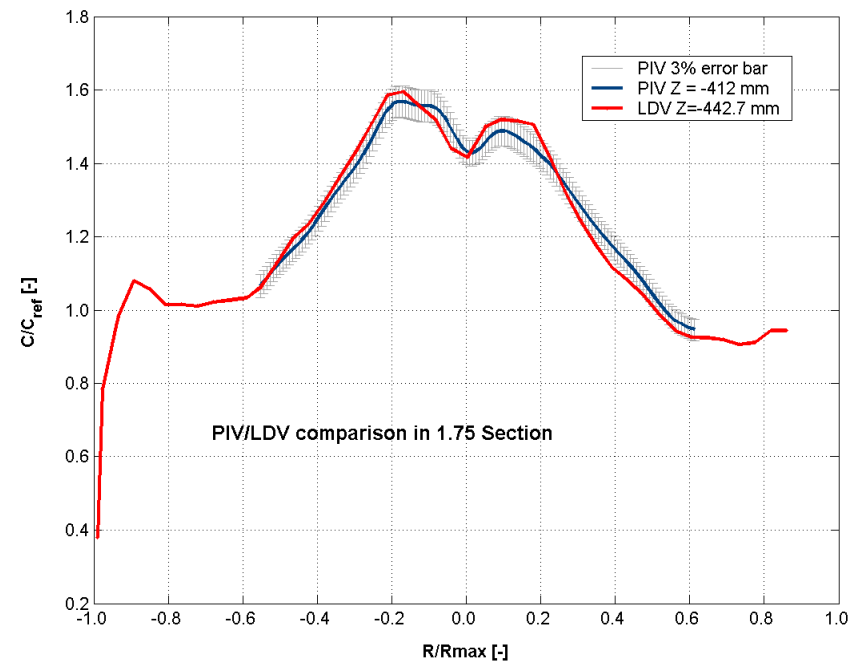
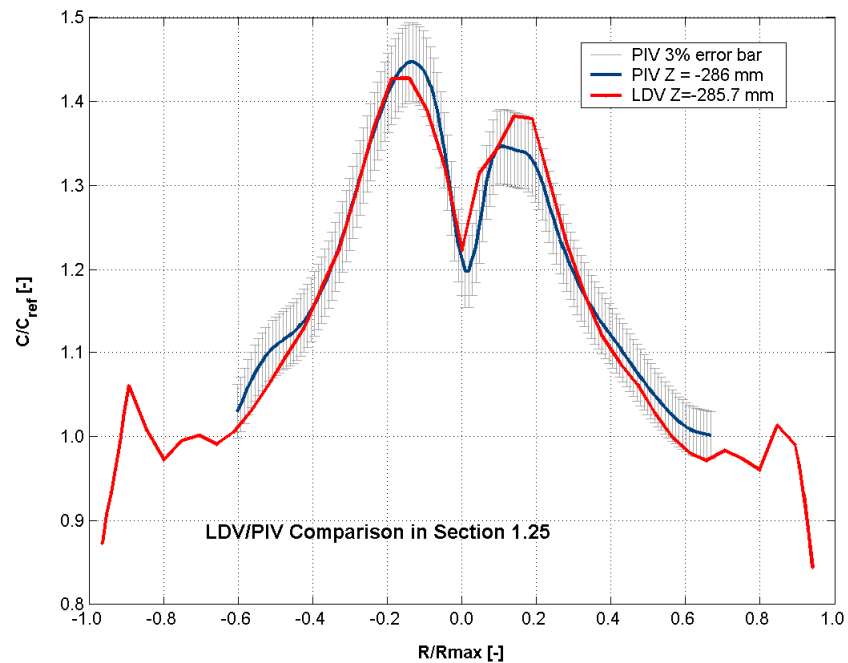


Ciocan G.D., Avellan F., "Flow Investigations in a Francis Draft Tube: Advanced Experimental Methods"
3rd Conference of Romanian Hydropower Engineers, Romania, 2004

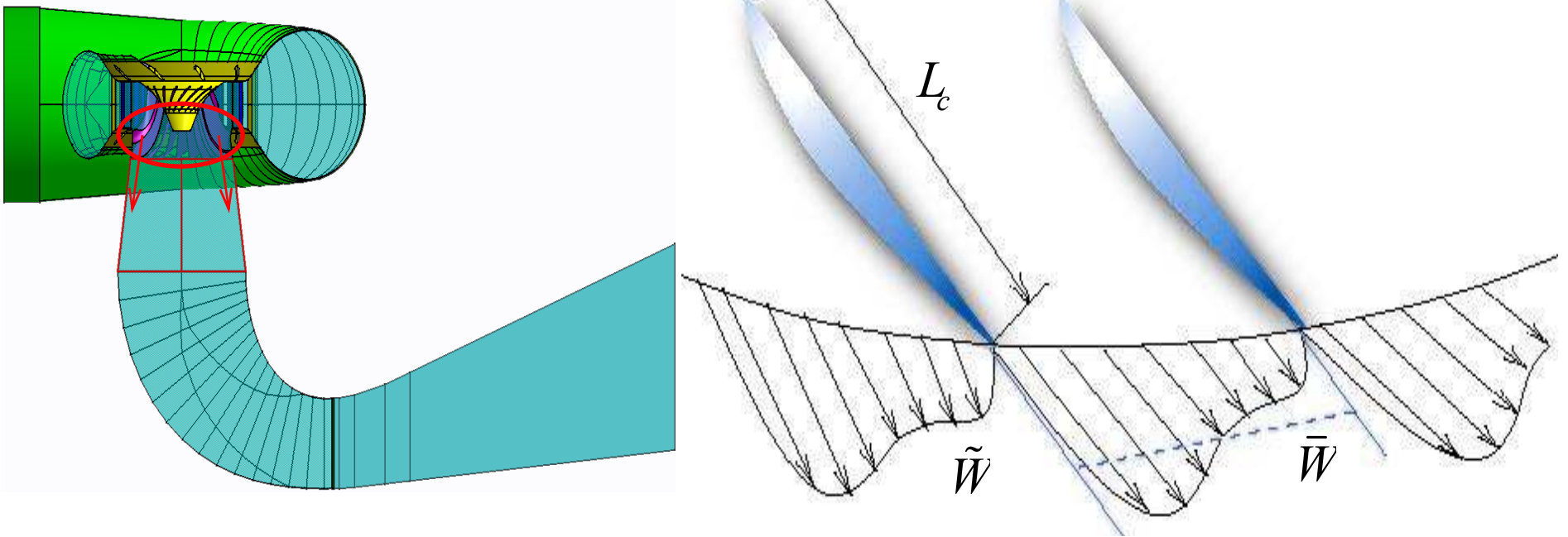
3D PIV in the Cone



3D Particle Image Velocimetry

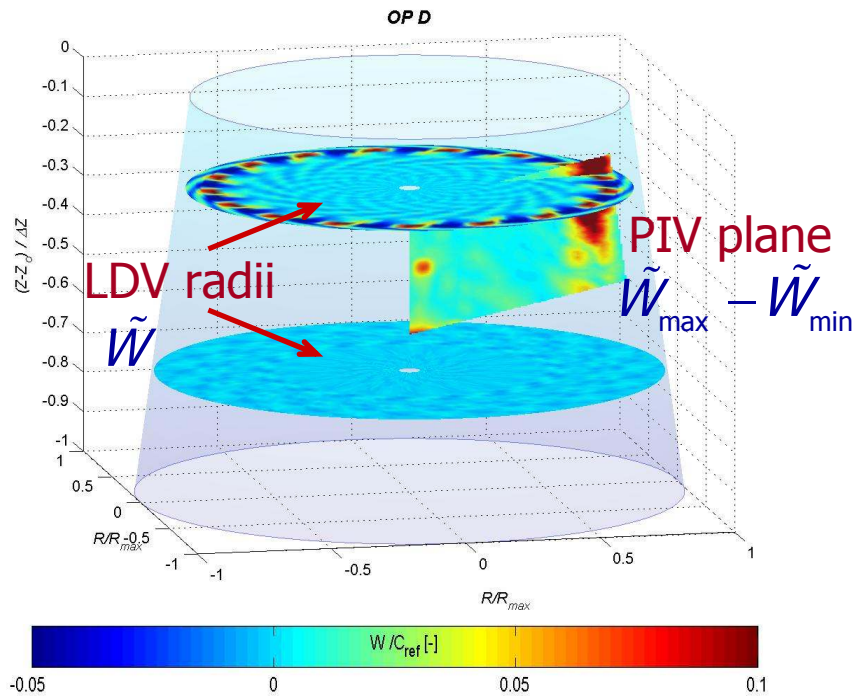


Sheared flow mixing



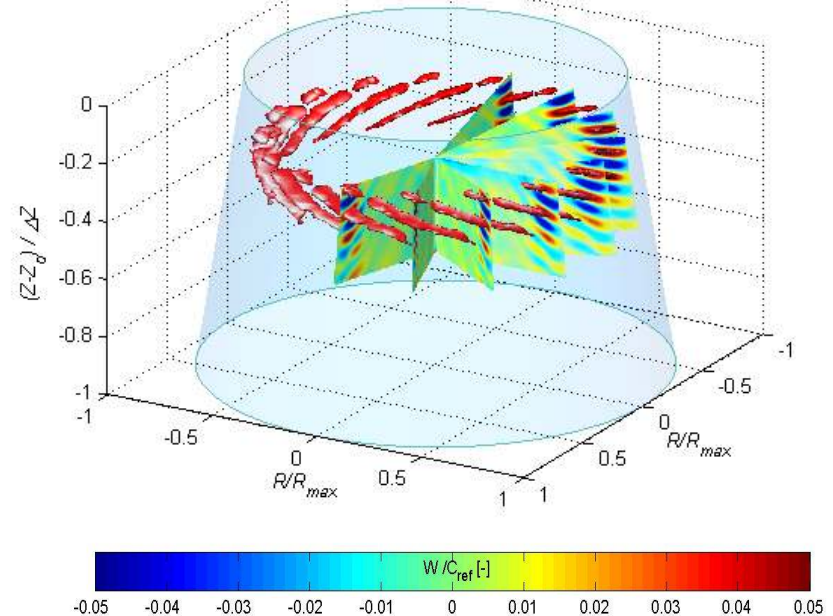
- Blade-to-blade flow field non-uniformity
- Pressure/suction side boundary layers shearing
- Led by the relative flow

Sheared flow mixing



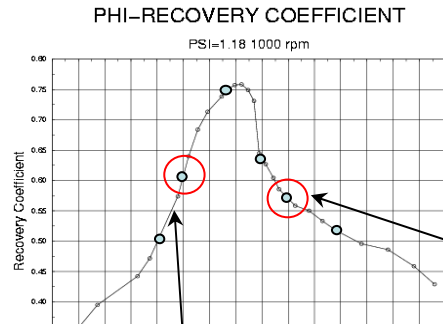
LDV – phase average velocity fields
PIV – fluctuation amplitude field

$$(\tilde{W}_{\max} - \tilde{W}_{\min}) / C_{ref} = k(L/L_c)^{-1}$$



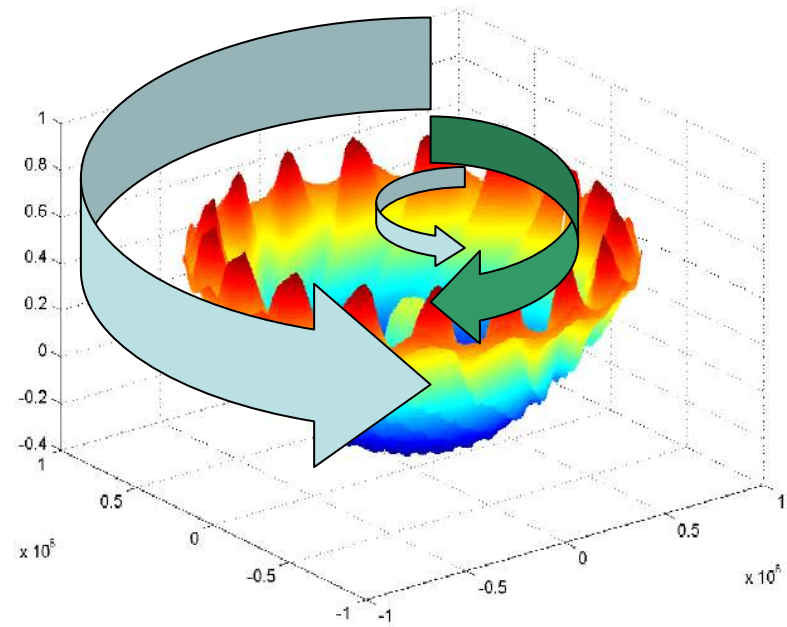
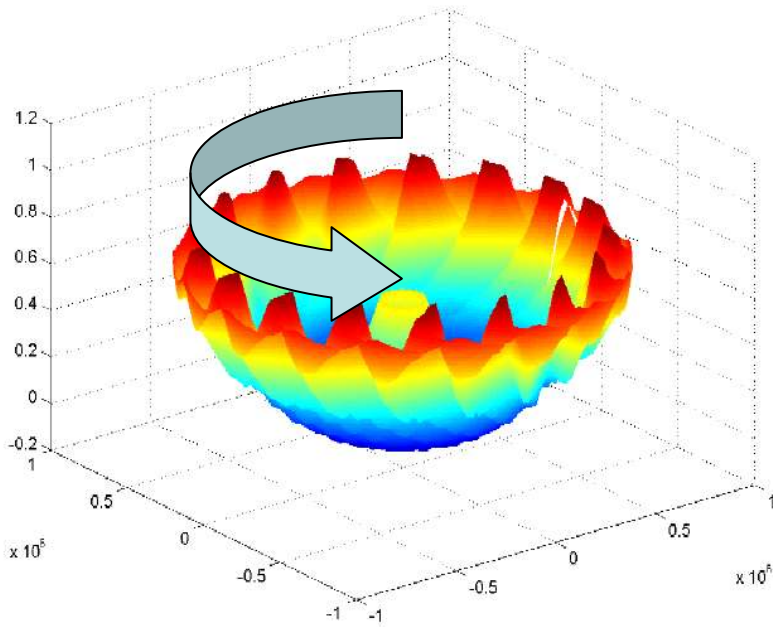
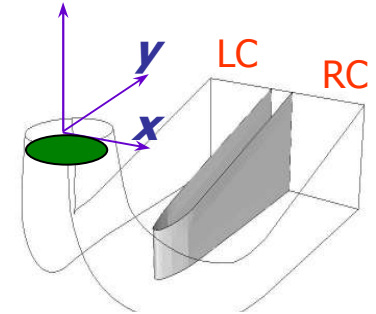
Blade-to-blade channel flow velocity
propagation & dispersal in the cone

LDV Runner Outlet – Phase Average



Unsteady
values

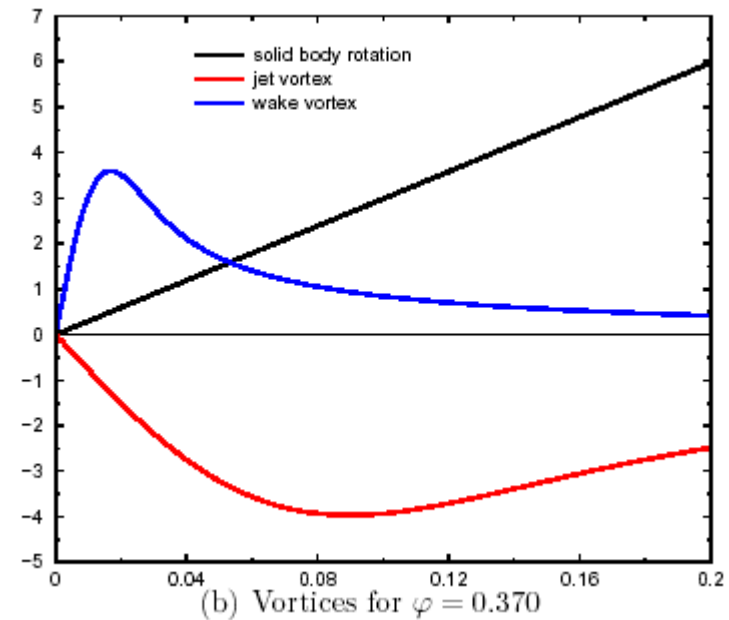
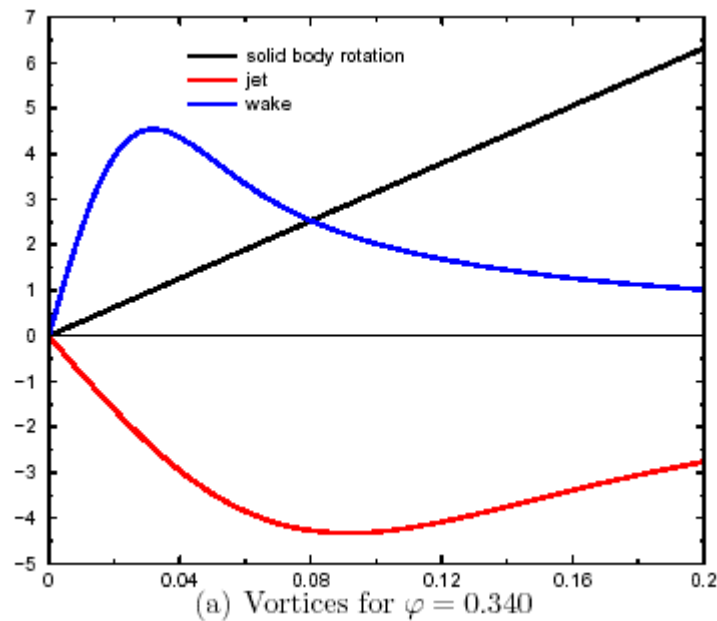
$$\tilde{c}_w^T + \overline{c}_w$$



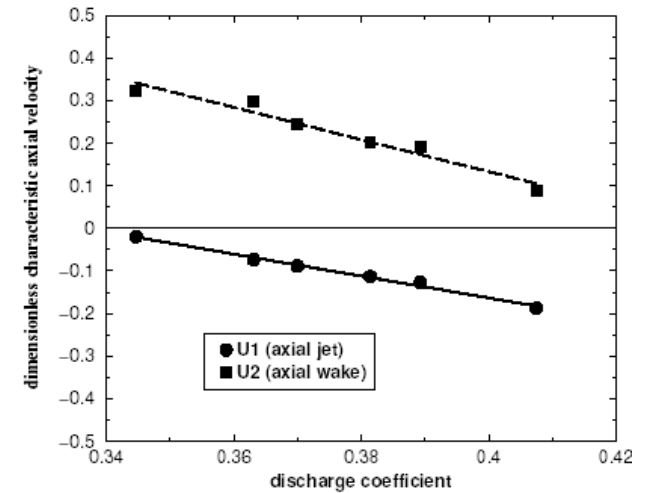
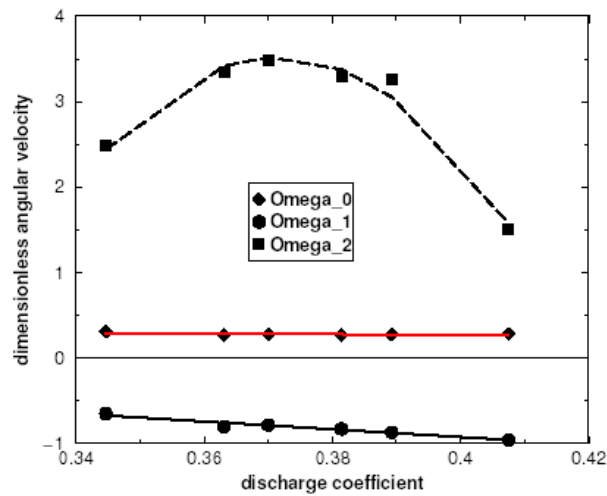
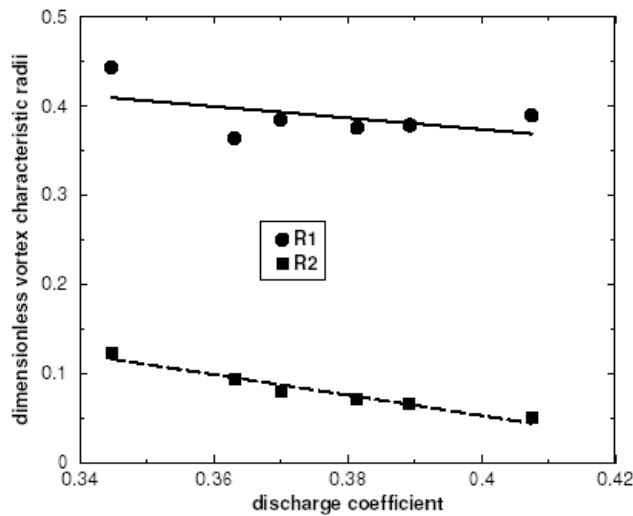
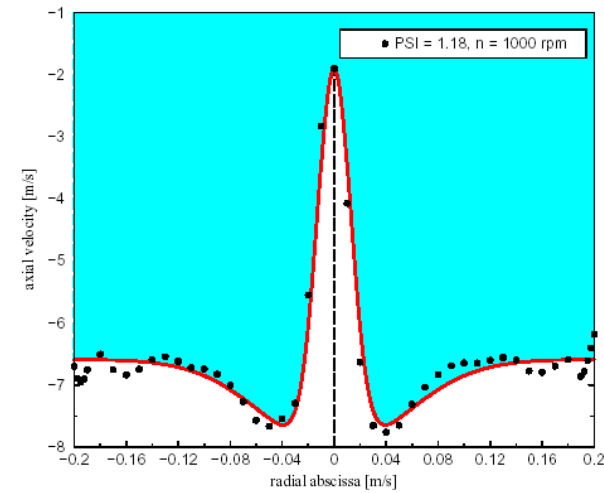
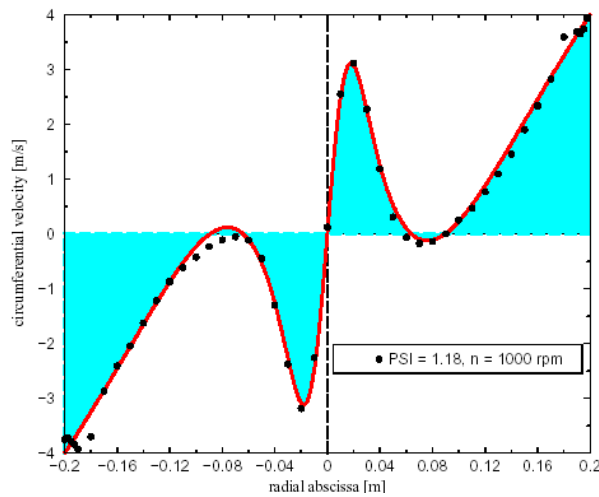
Analytical Description of the Velocity Profile

$$v_u = \Omega_0 r + \Omega_1 \frac{R_1^2}{r} \left[1 - \exp\left(-\frac{r^2}{R_1^2}\right) \right] + \Omega_2 \frac{R_2^2}{r} \left[1 - \exp\left(-\frac{r^2}{R_2^2}\right) \right] \quad (1)$$

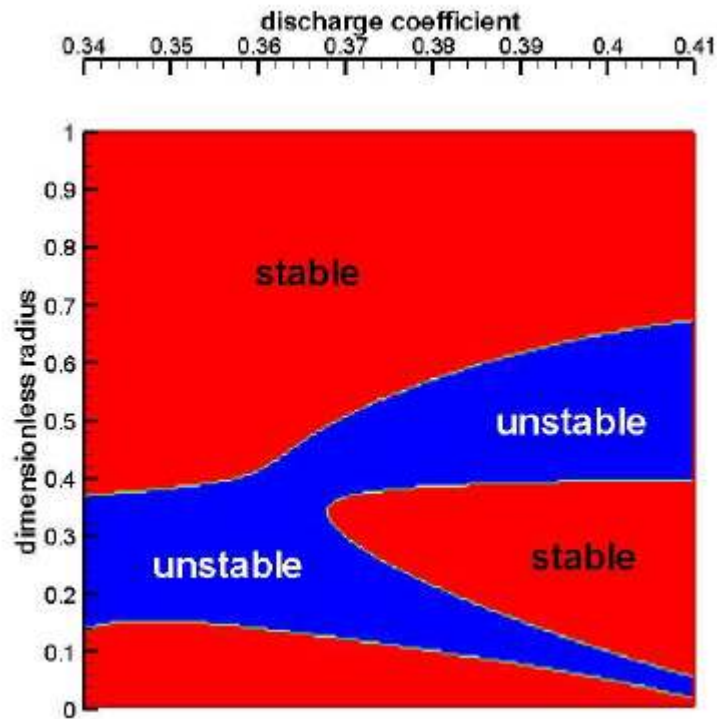
$$v_a = U_0 + U_1 \exp\left(-\frac{r^2}{R_1^2}\right) + U_2 \exp\left(-\frac{r^2}{R_2^2}\right) \quad (2)$$



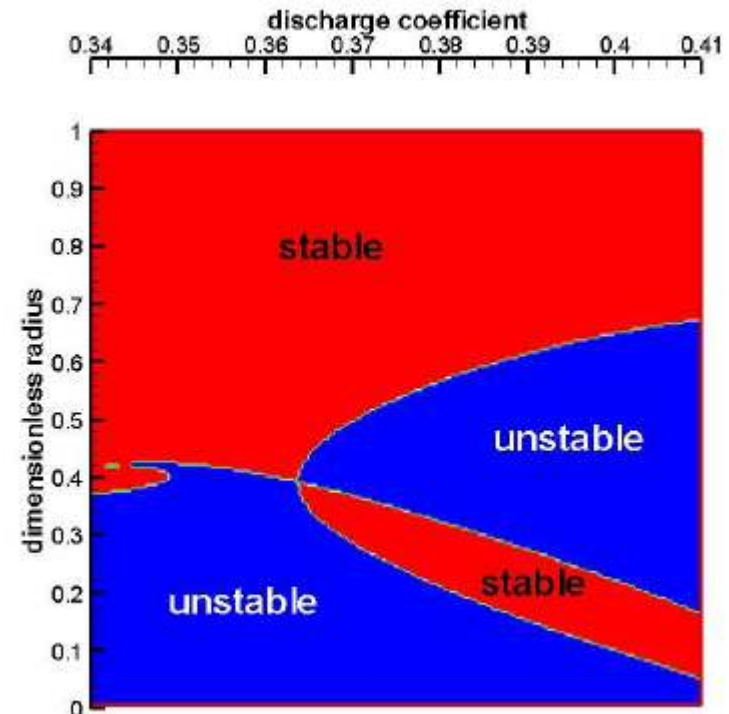
Analytical Description of the Velocity Profile



Étude de stabilité du profile de vitesse



Critère de stabilité Howard-Gupta
Perturbation axisymétrique



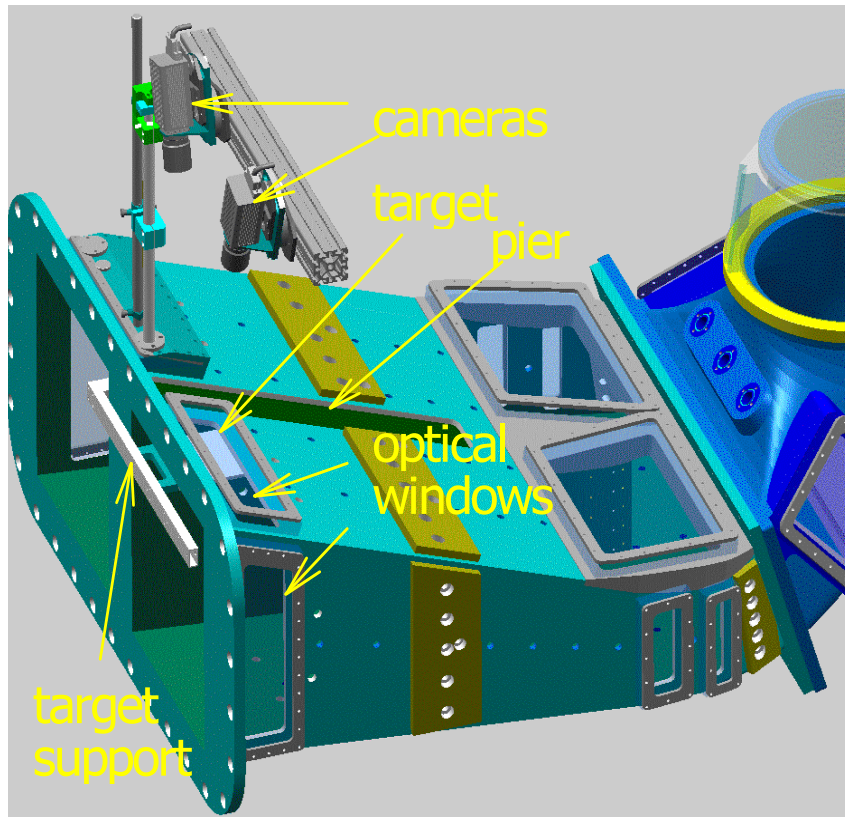
Critère de stabilité Leibovich-Stewartson
Perturbation non axisymétrique

Accuracy

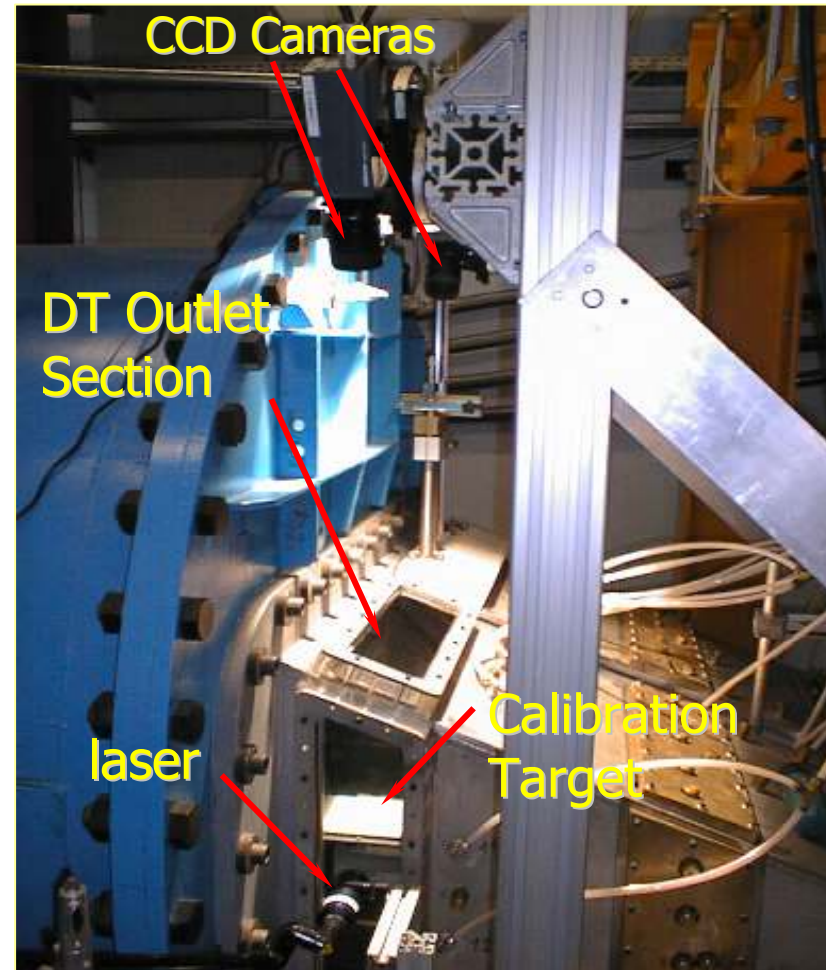
Measured discharge	Energy Coeff.	Speed [rpm]	Computed discharge	Error [%]
0.340	1.18	1000	0.344	+1.1
0.360	1.18	1000	0.363	+0.8
0.368	1.18	1000	0.372	+1.0
0.380	1.18	1000	0.381	+0.2
0.390	1.18	1000	0.389	-0.2
0.410	1.18	1000	0.409	-0.3
0.368	1.00	1000	0.368	+0.1
0.380	1.00	1000	0.380	+0.1
0.370	1.11	1000	0.369	-0.1
0.368	1.30	1000	0.371	+0.8
0.380	1.30	1000	0.386	+1.5
0.410	1.30	1000	0.407	-0.6
0.370	1.11	500	0.370	+0.1
0.340	1.18	500	0.345	+1.6
0.368	1.18	500	0.369	+0.2
0.380	1.18	500	0.379	-0.3
0.410	1.18	500	0.406	-0.9

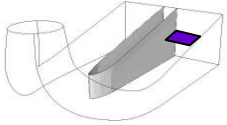
- Discharge computed from fitted axial velocity profile agrees within less than 1% with the measured discharge
- The energy coefficient does not influence the velocity profiles at constant discharge
- Reynolds number effect is negligible (same velocity profiles at different runner speed)

3D-PIV Draft Tube Outlet

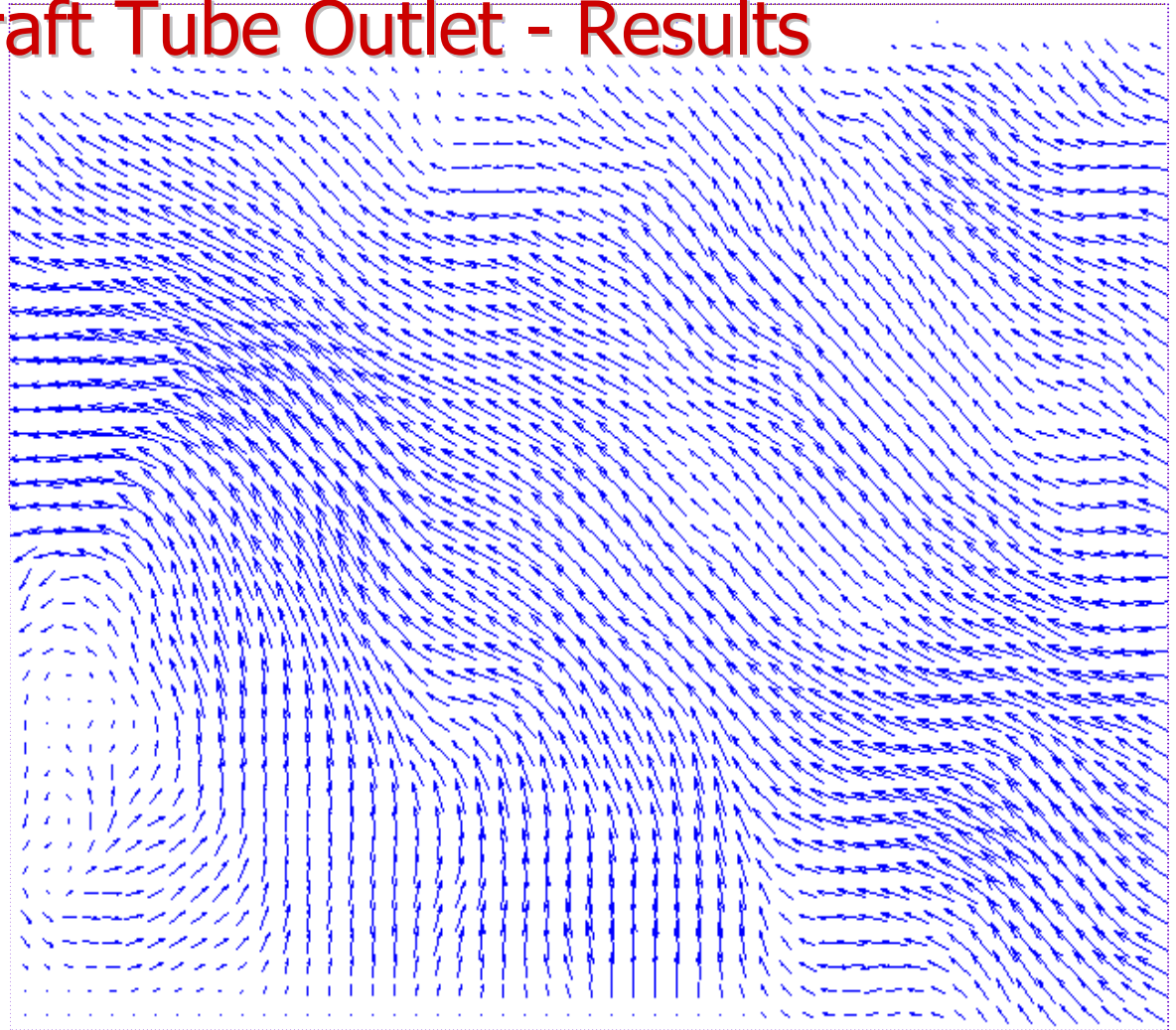
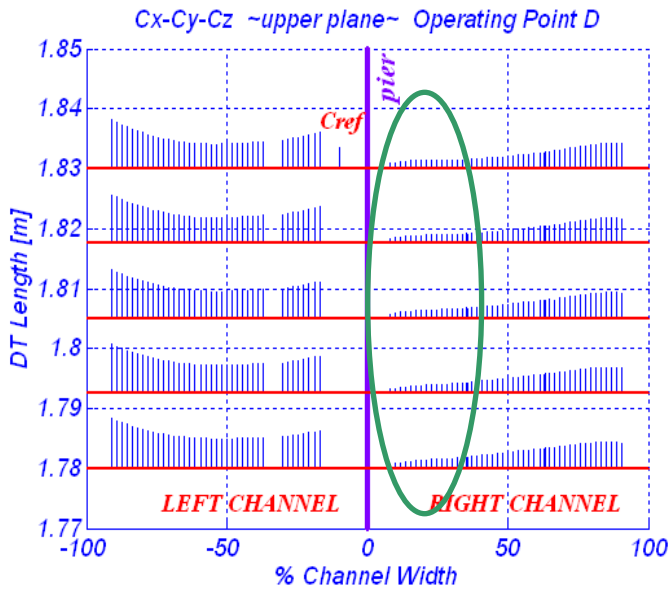
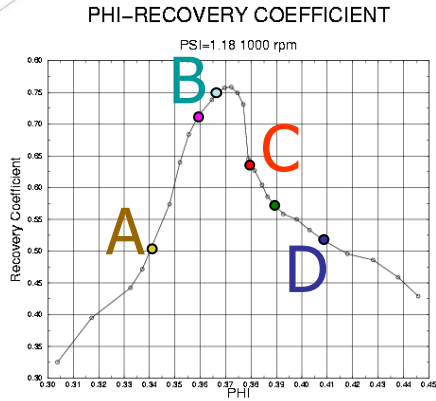


Experimental Setup



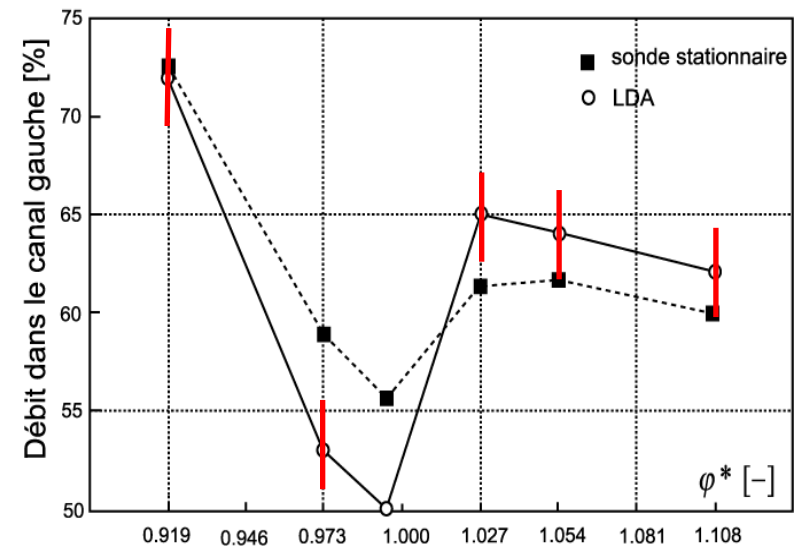
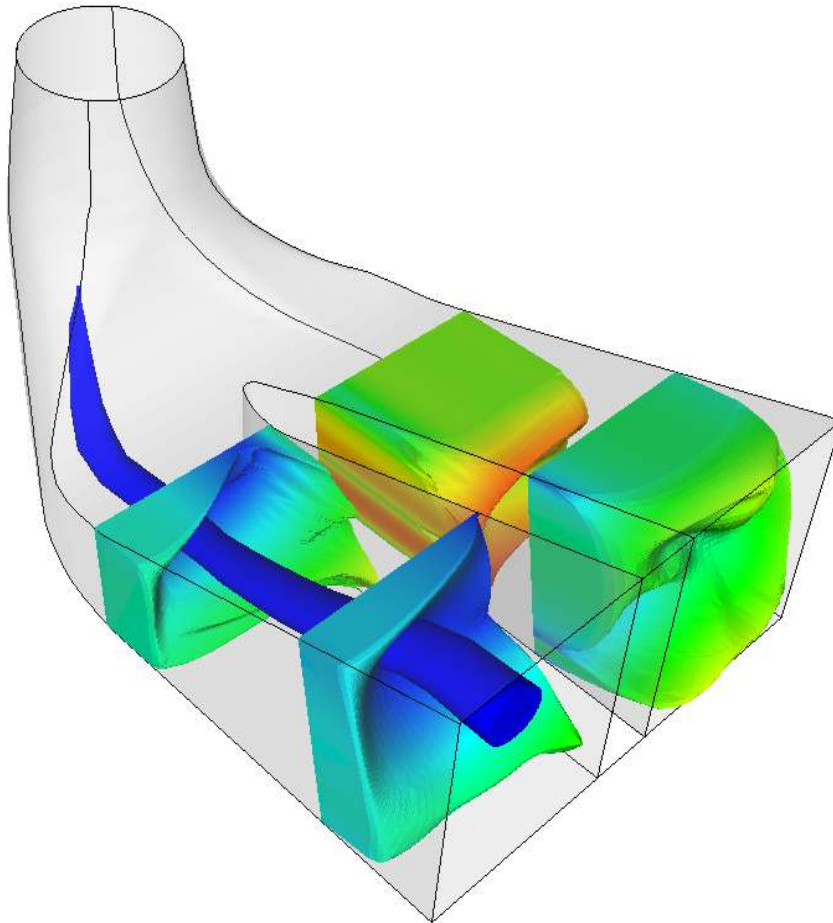


3D-PIV Draft Tube Outlet - Results



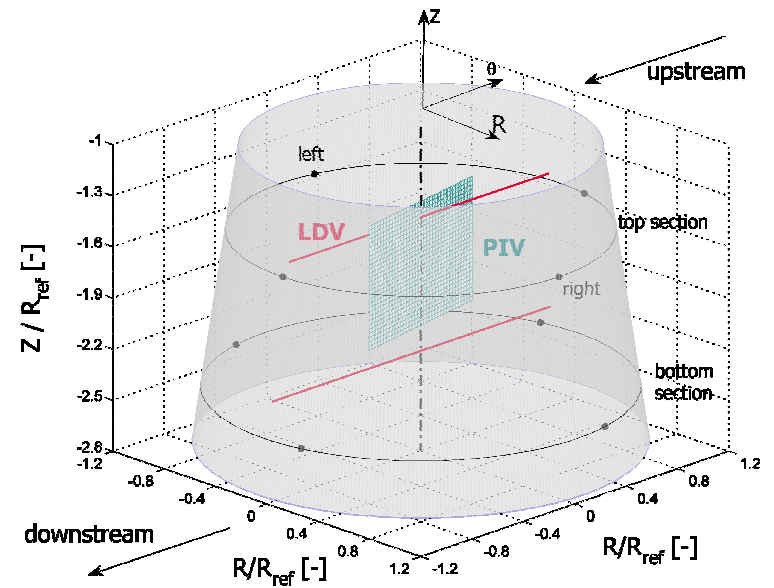
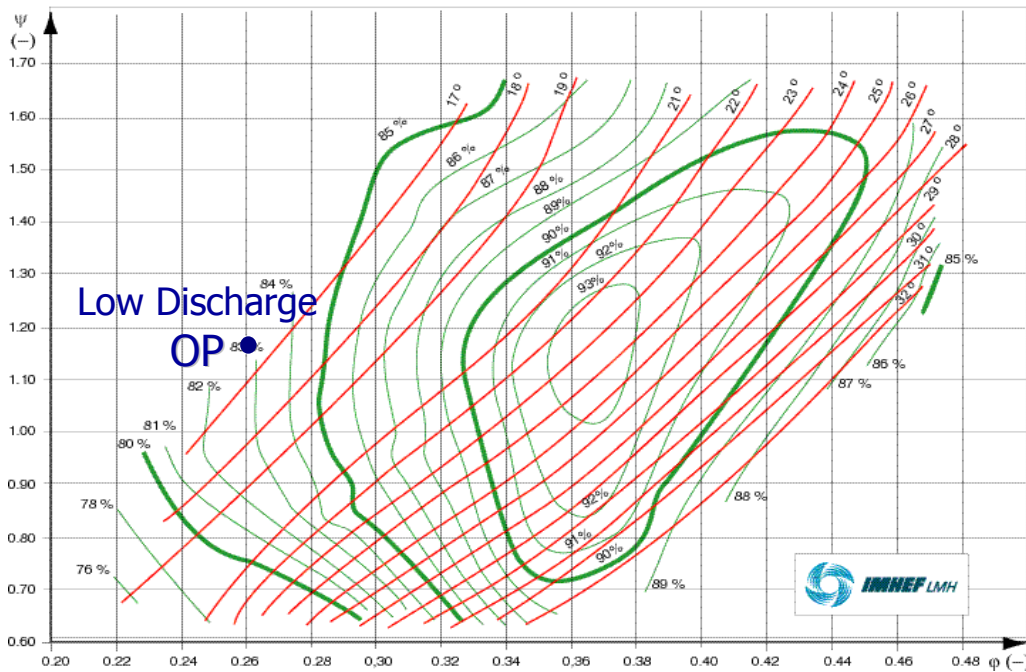
Instantaneous 2D Vector Fields

Flow rate distribution

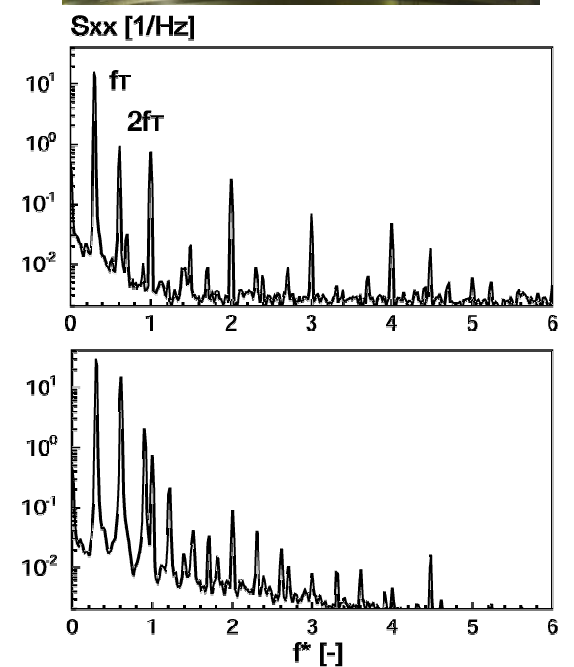
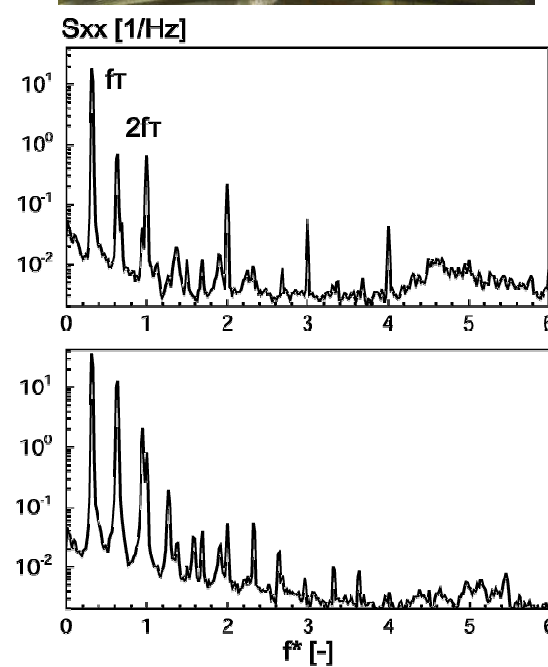
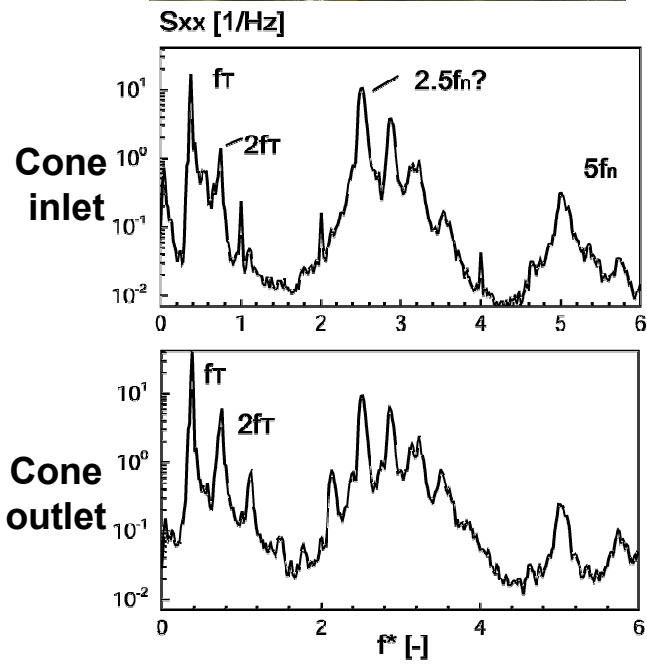
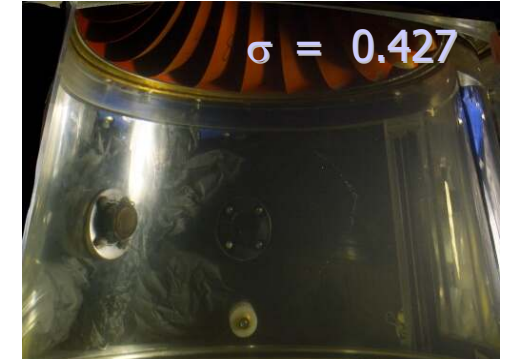
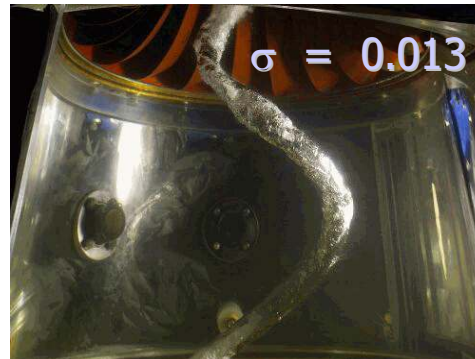
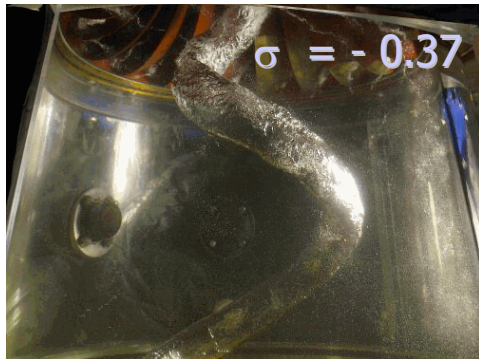


Accuracy of the flow rate
estimation: $\sim 4\%$

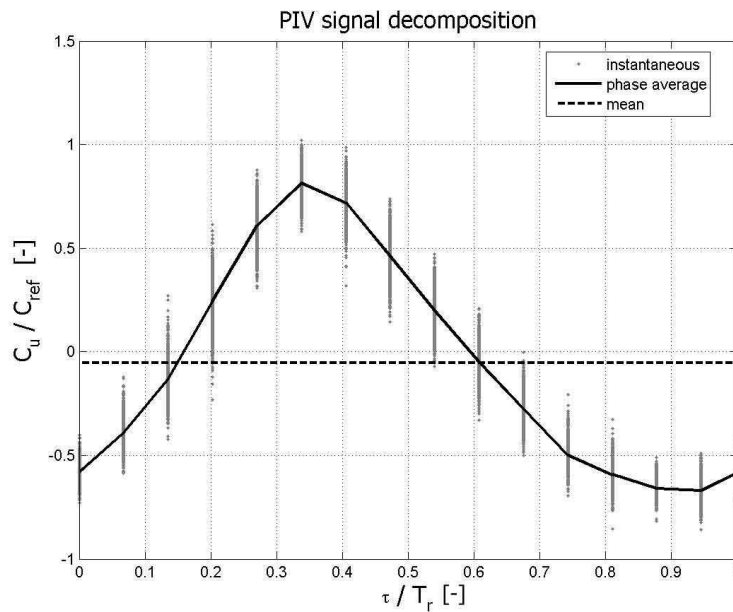
Partial Flow Rate Operating Point



Unsteady Pressure Field



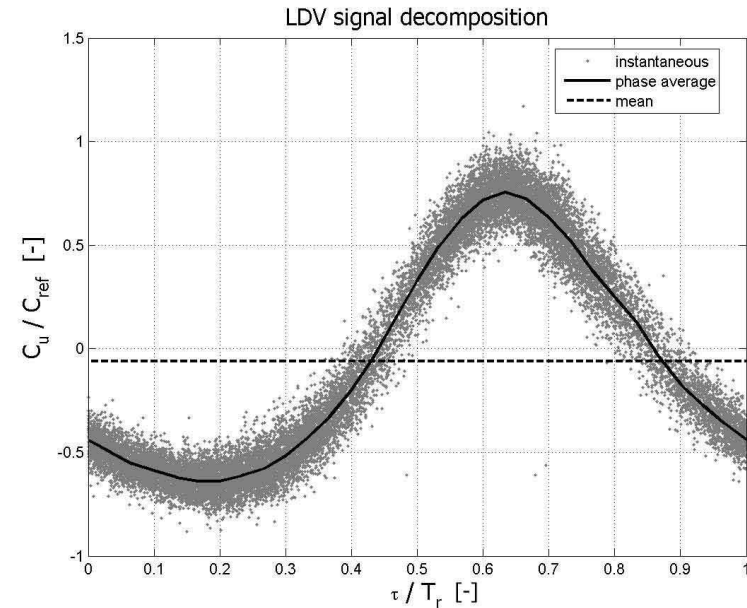
Phase Average on the Rope Passage



Phase average - PIV

$$C_i(t) = \bar{C} + \tilde{C}(\tau) + C'(t)$$

$$\bar{C} = \langle C_i \rangle = \lim_{N \rightarrow \infty} \frac{1}{N} \sum_{i=1}^N C_i(t)$$



Phase average - LDV

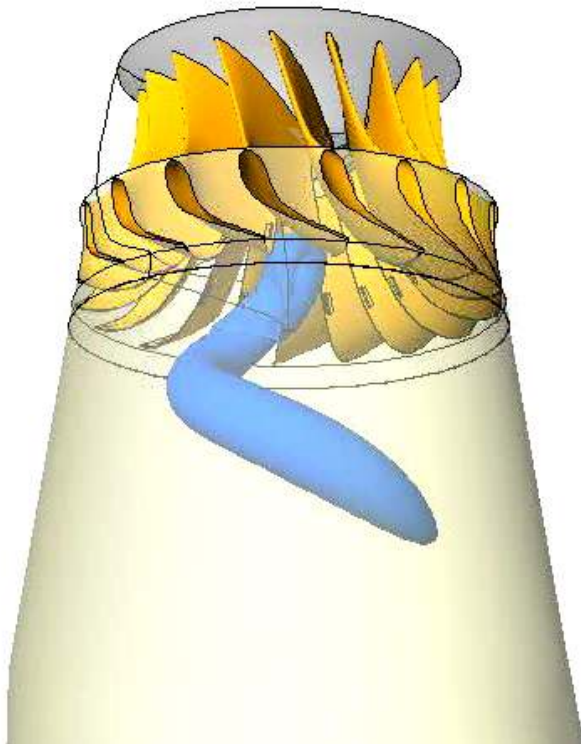
$$\tilde{C}(\tau) = \lim_{N' \rightarrow \infty} \frac{1}{N'} \sum_{i=1}^{N'} (C_i(\tau) - \bar{C})$$

$$\bar{\tilde{C}} = 0$$

$$\langle C' \rangle = \lim_{N \rightarrow \infty} (C_i(t) - \bar{C} - \tilde{C}) = 0$$

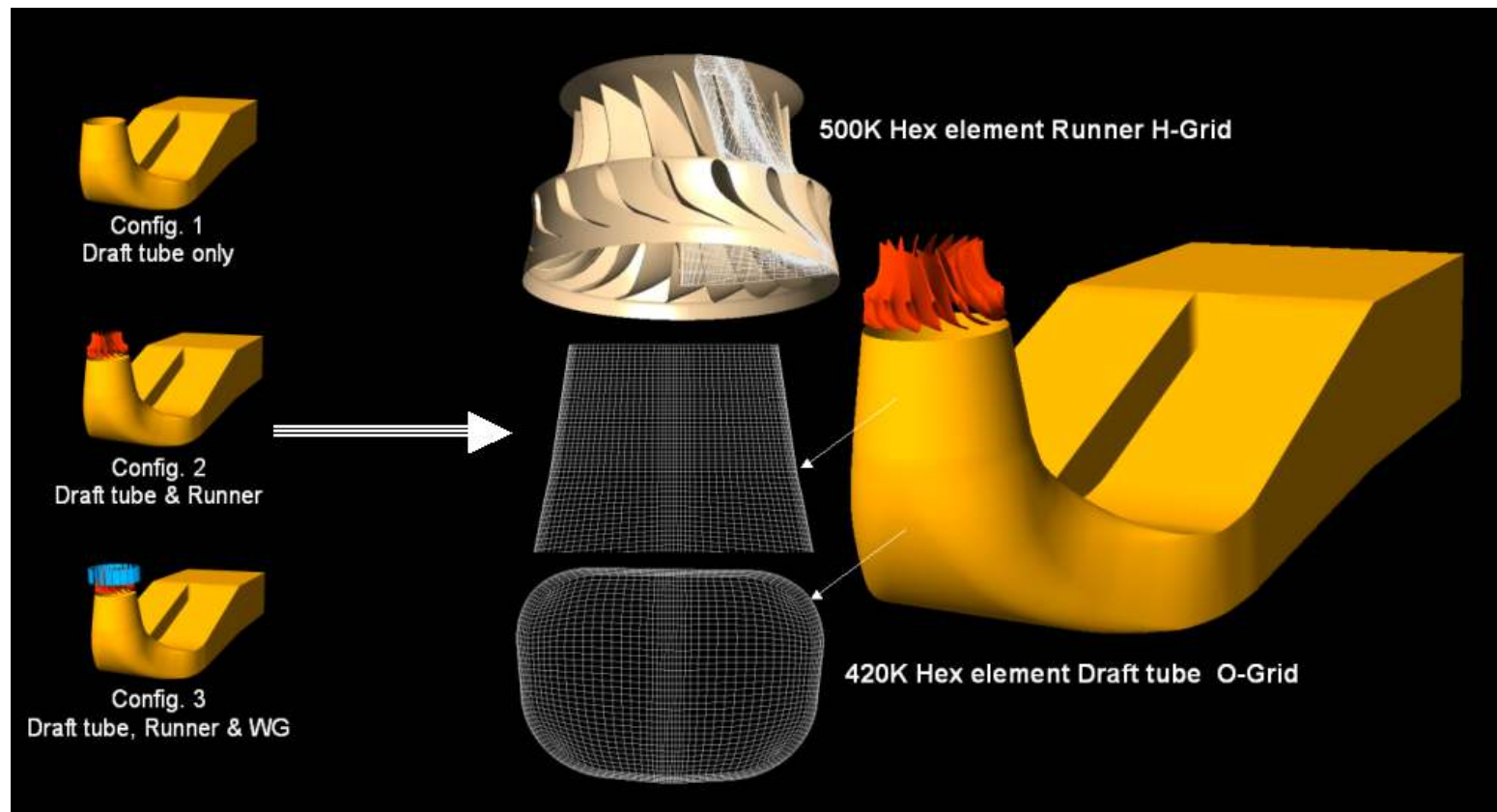
Unsteady Simulation of Rotating Rope

time = 0.00000



–Vortex rope without vapors

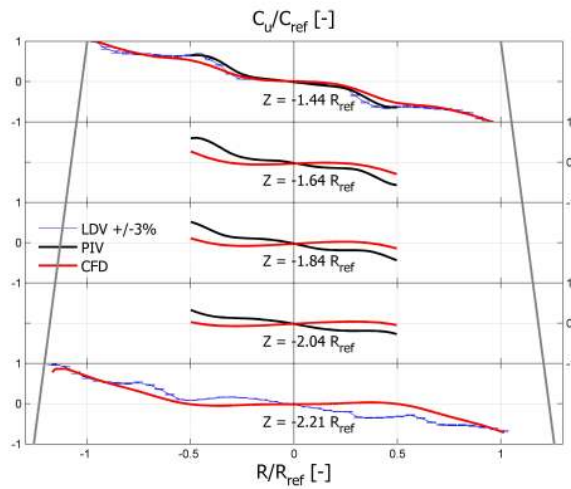
Computation Flow Domain & Mesh



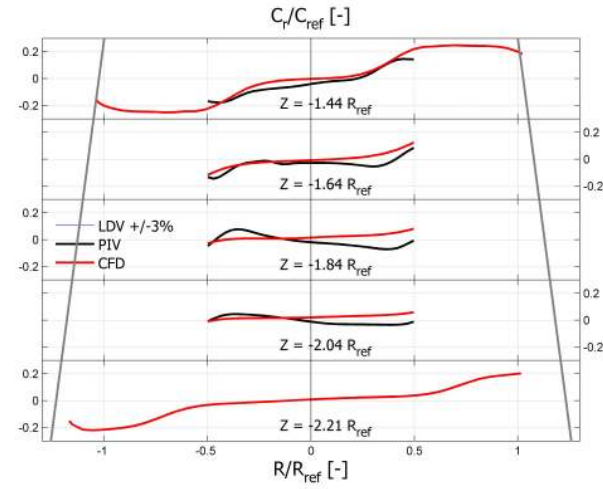
1.2 million node multi-block structured mesh
Inlet condition obtained from previous stage
calculation

Average Velocity Profiles

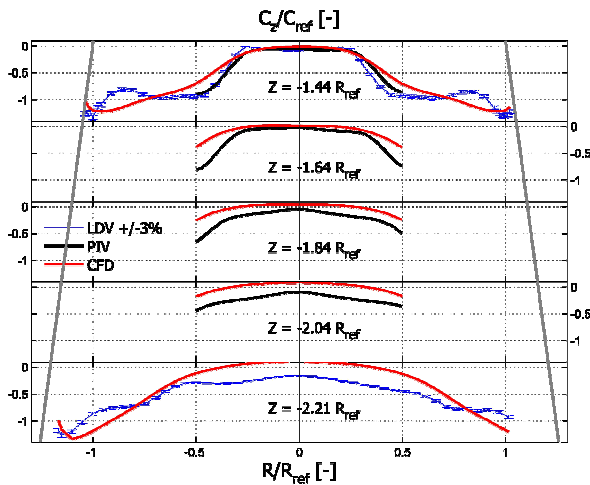
C_u



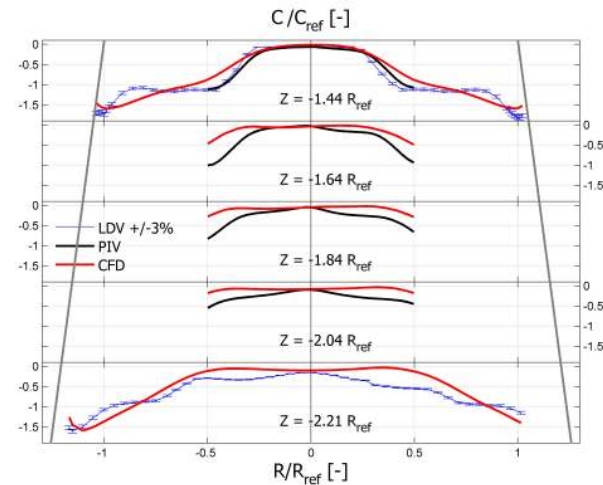
C_r



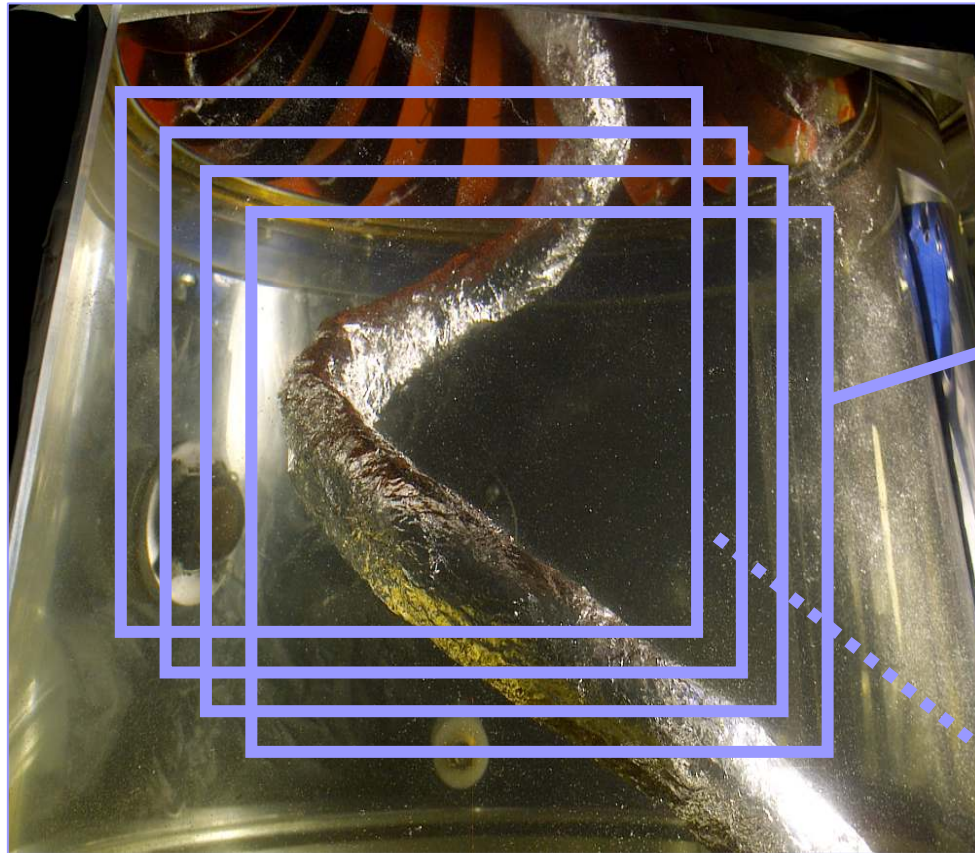
C_z



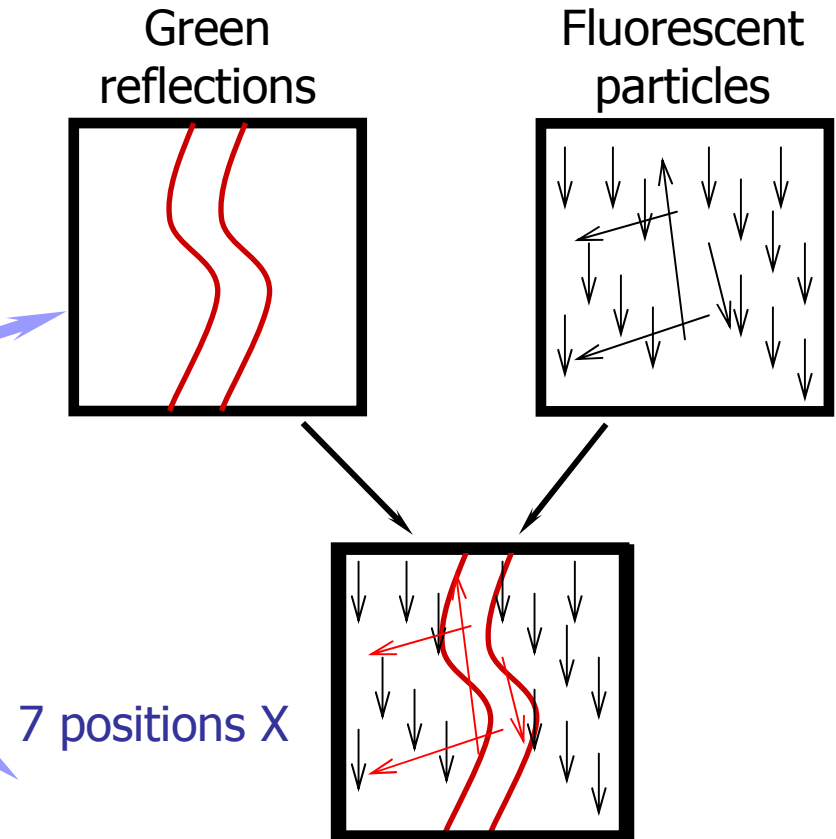
C



PIV 2phases - Principle

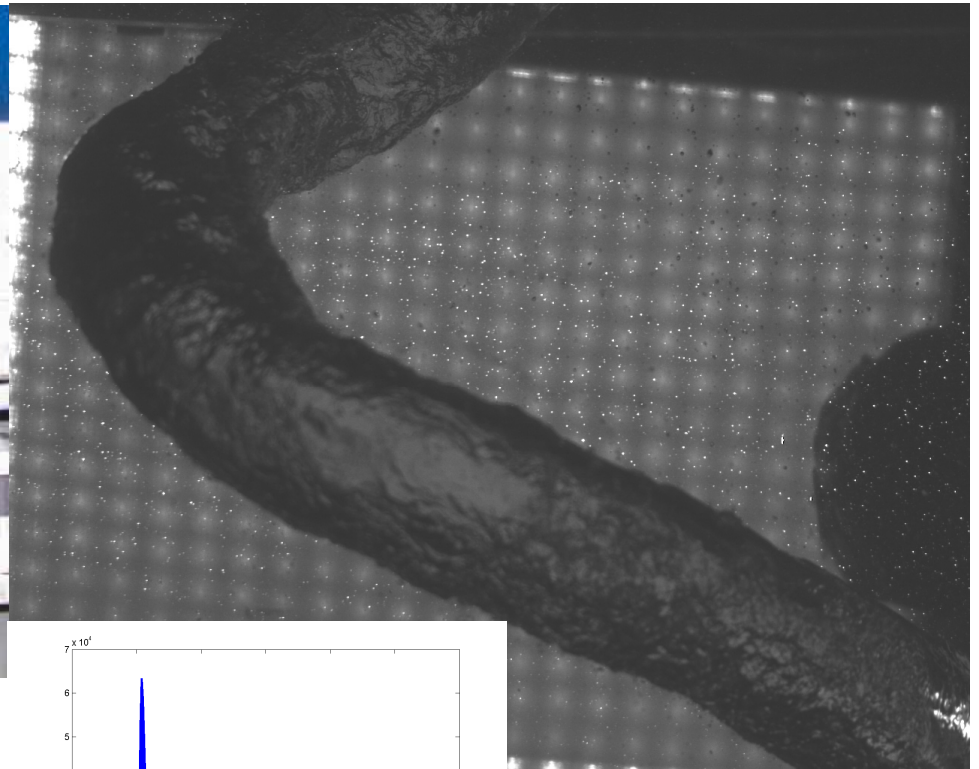


Synchronous with pressure signal for
different azimuthal positions of the rope

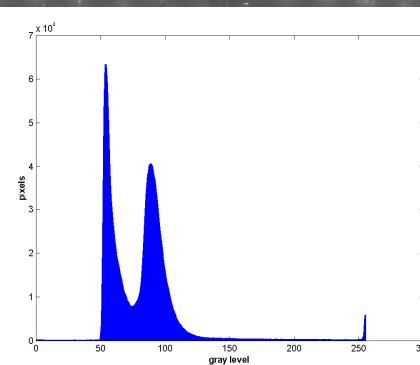


*Rope shape
+
2D velocity field*

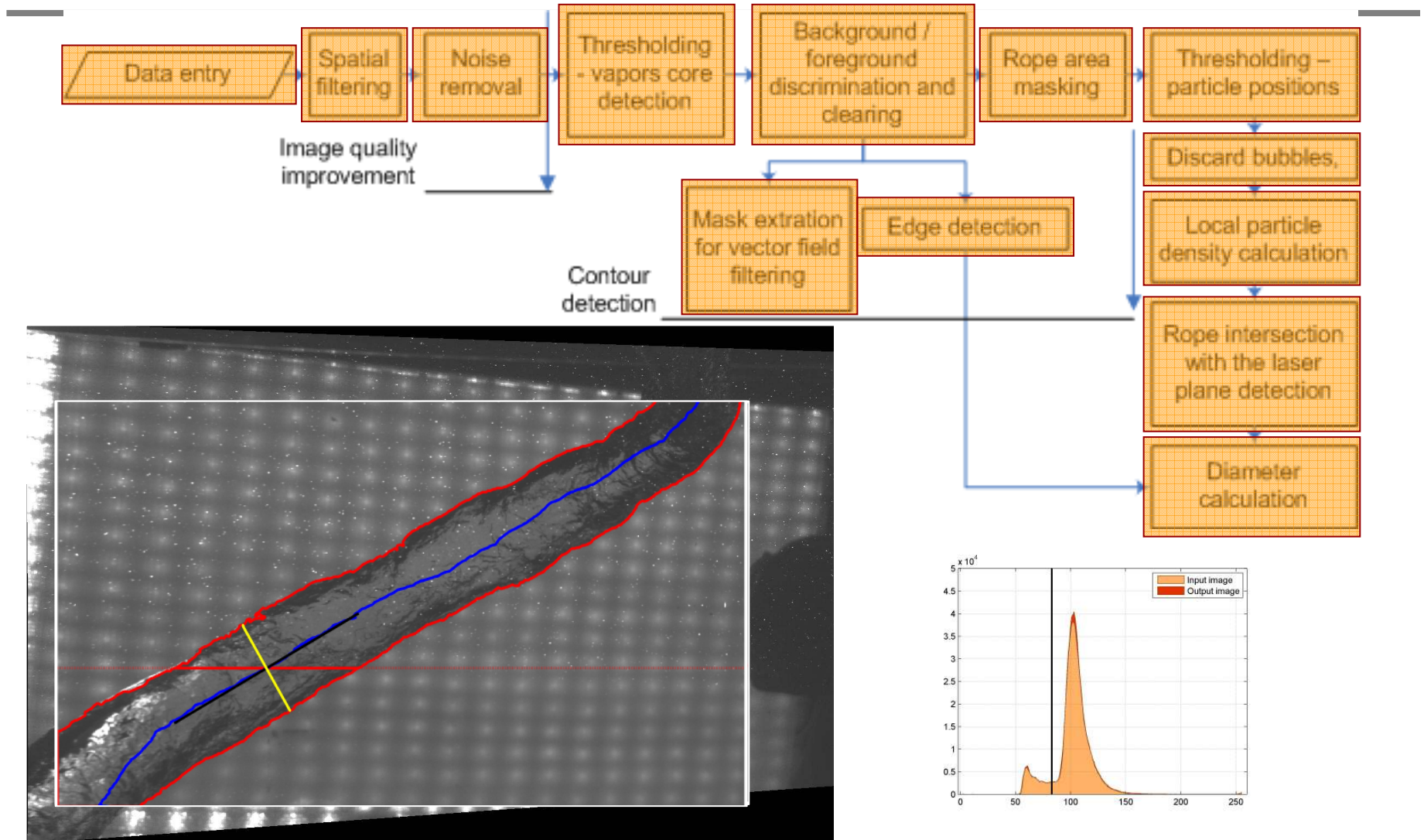
3D 2phase PIV



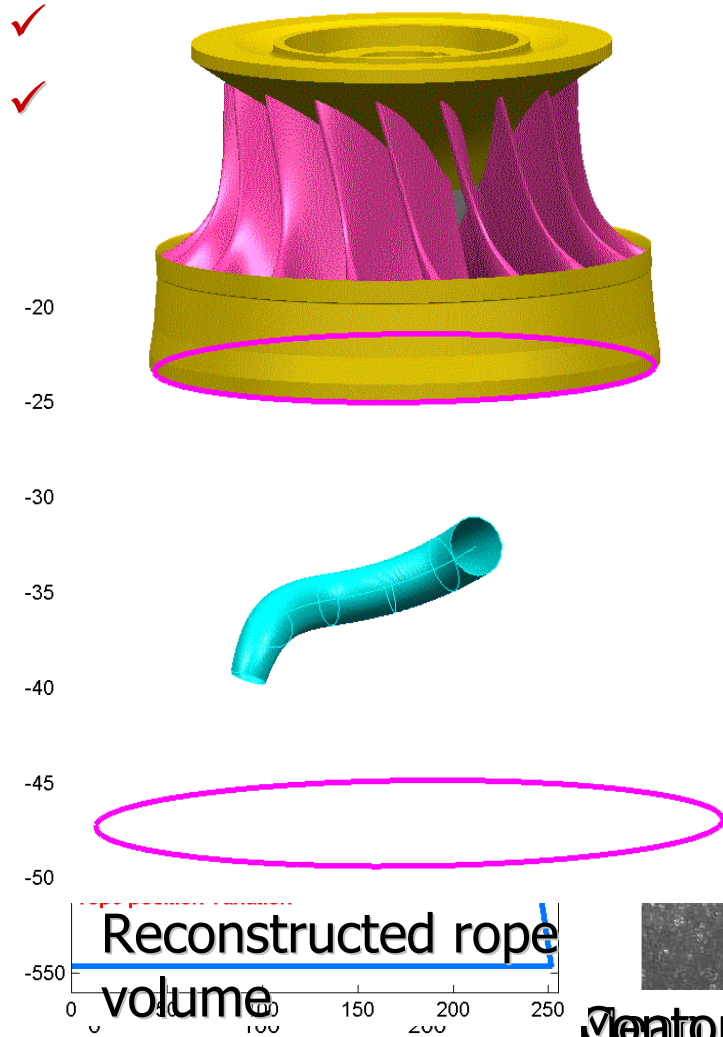
- Laser 532 nm
- LED 587 nm
- fluorescent particles 580 nm
- filters >570 nm



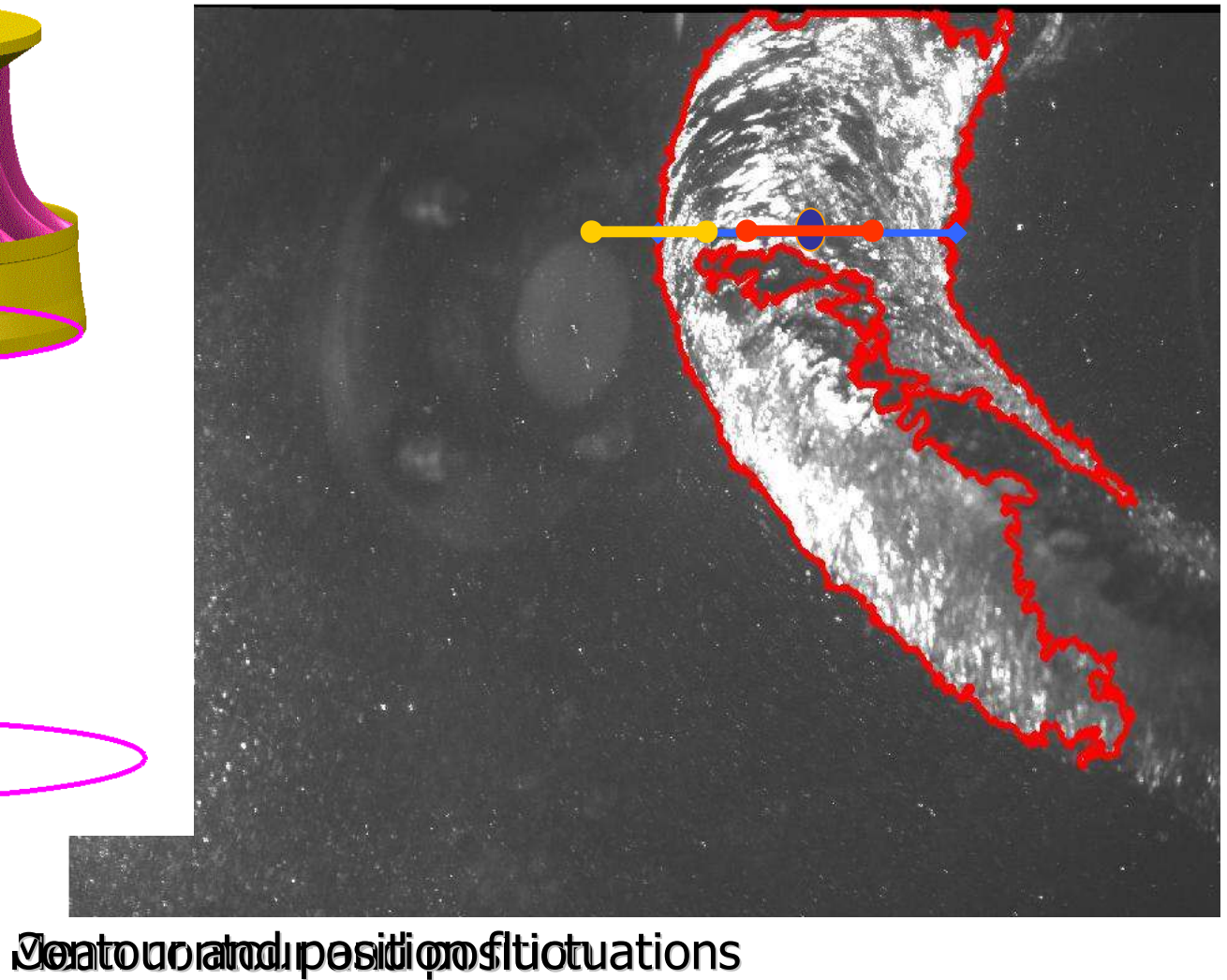
Metode moderne pentru cercetarea in Masini Hidraulice



Contour Validation Criteria

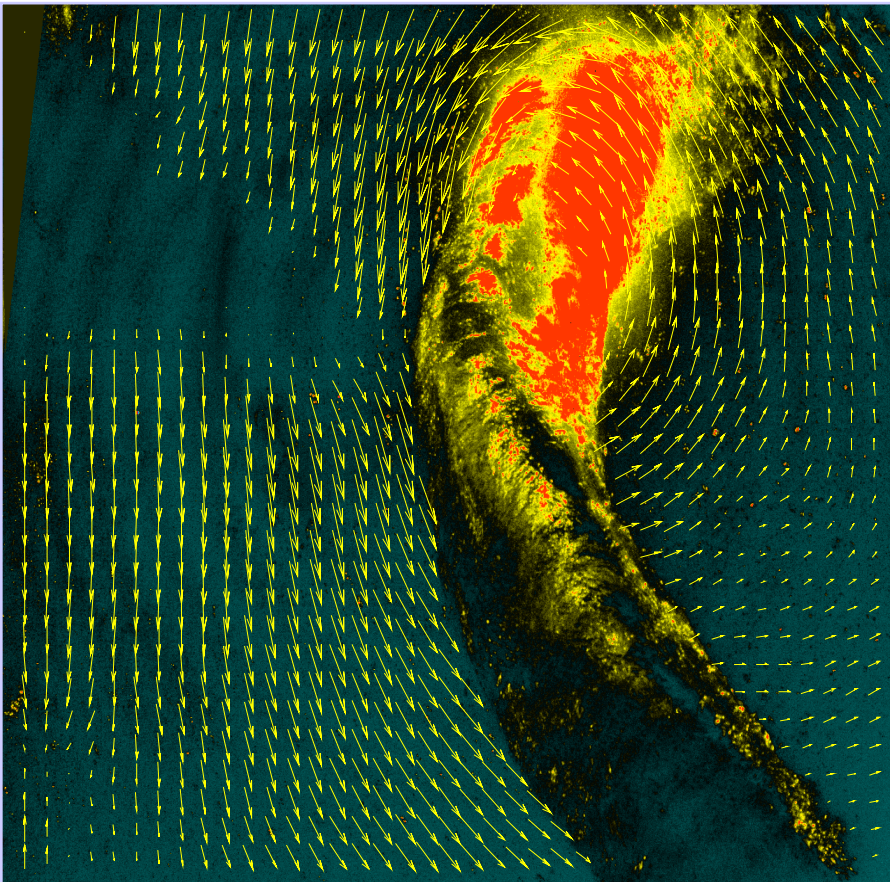


Rope Dynamics



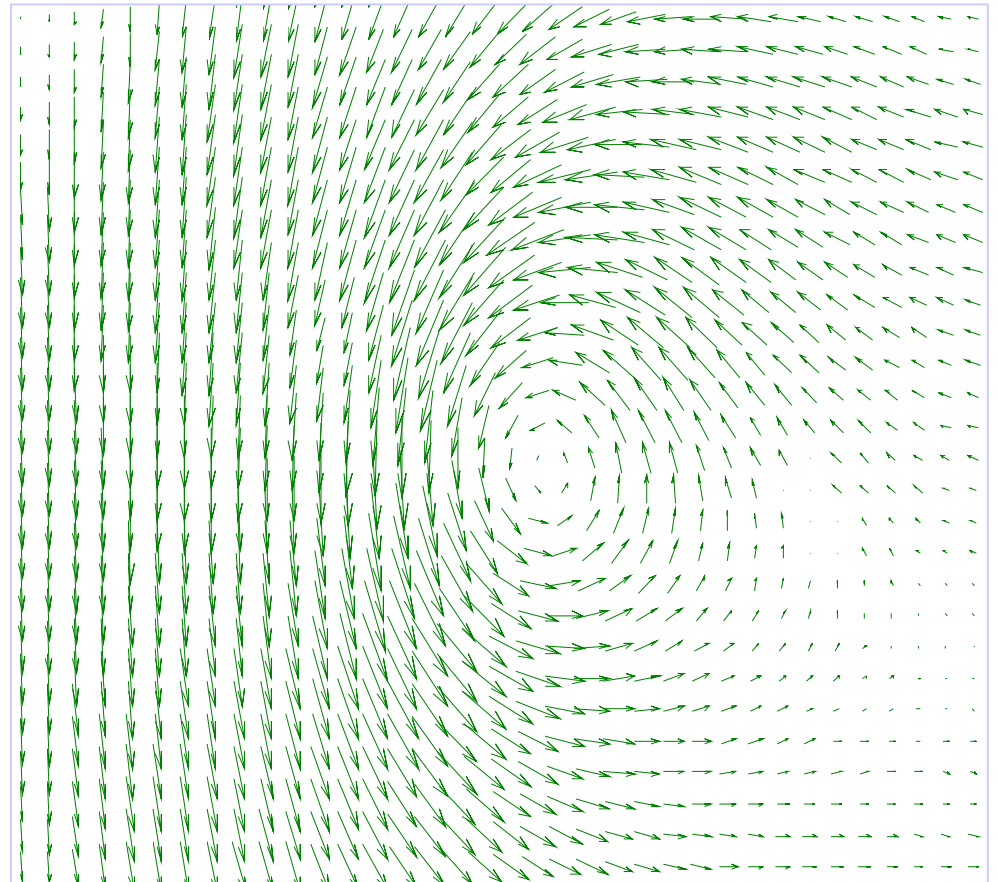
Sample Results

$\sigma = -0.370$



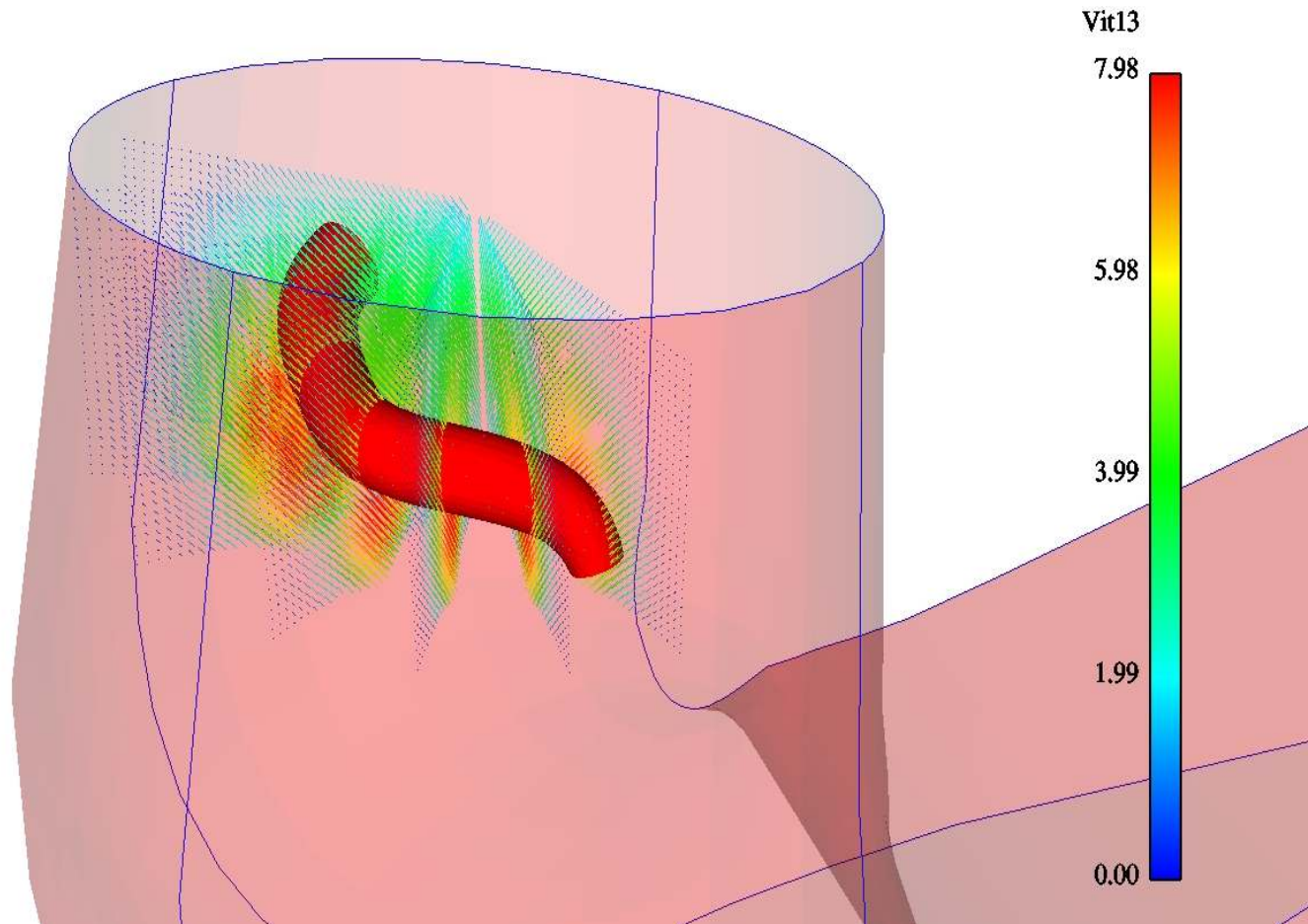
Rope Configuration

$\sigma = +0.427$



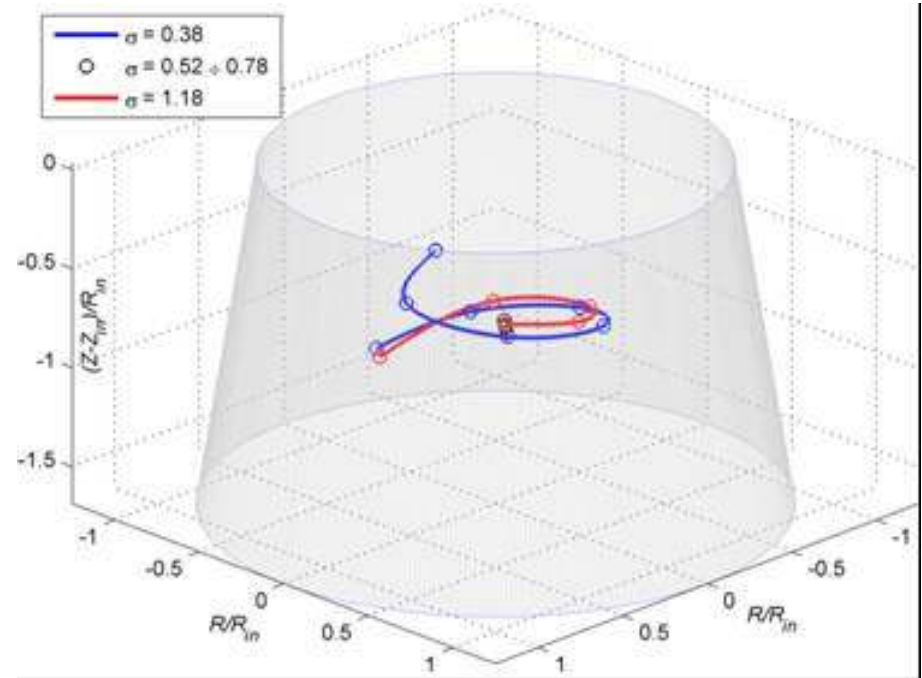
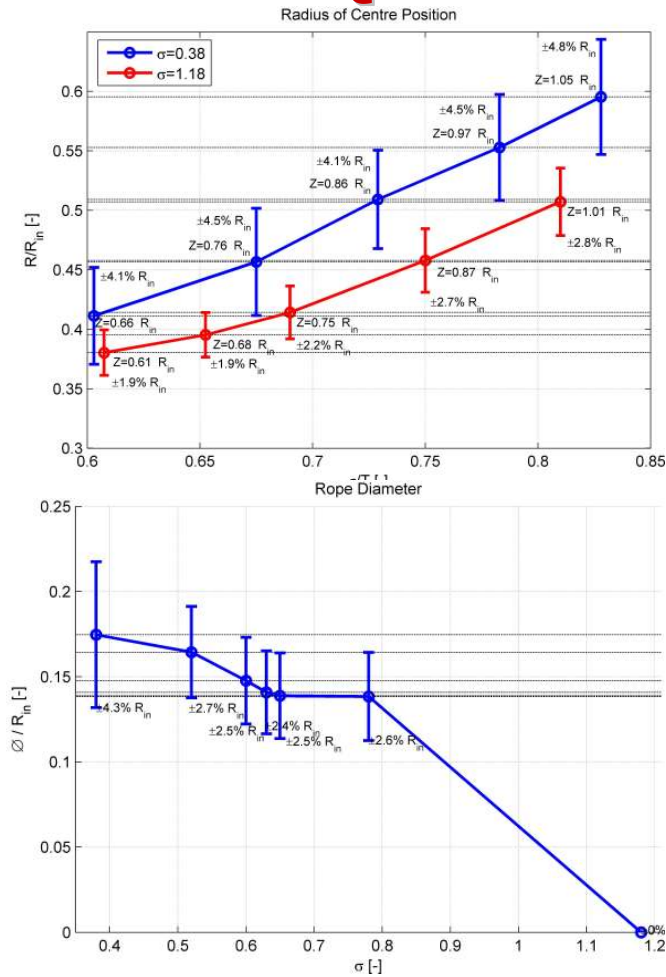
Vortex Configuration

Phase Average Reconstruction



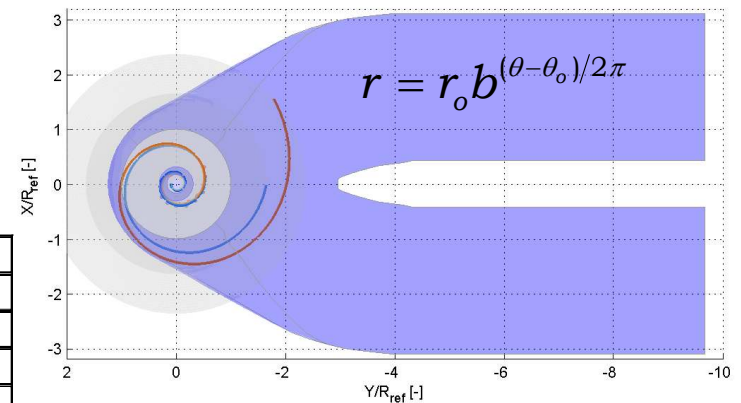
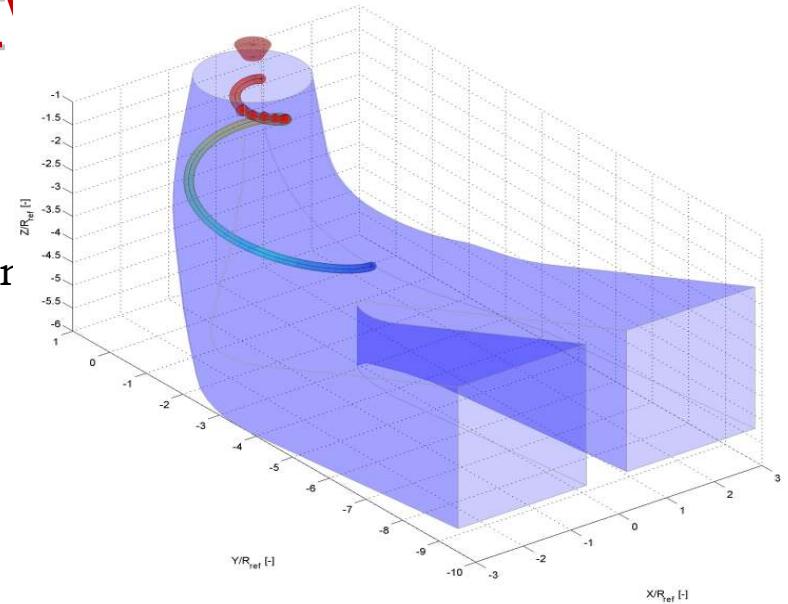
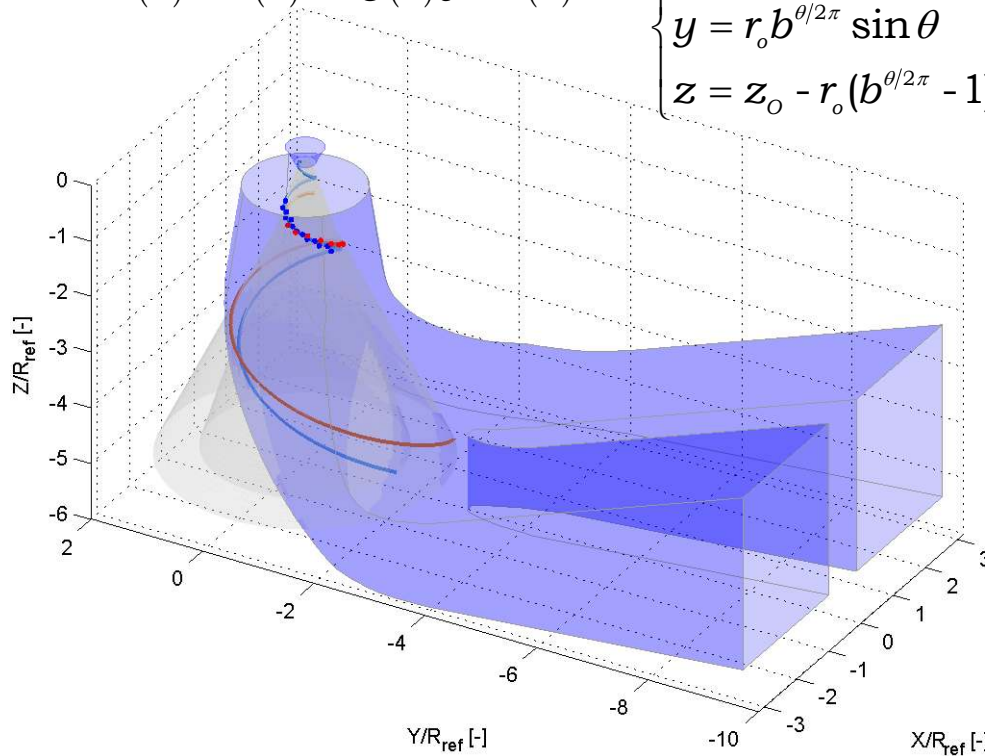
Iliescu M.S., Ciocan G.D., Avellan F.; "Two Phase PIV Measurements of a Partial Flow Rate Vortex Rope in a Francis Turbine"
- proposed for Journal of Fluids Engineering, 2006

Quantitative Rope Characterization



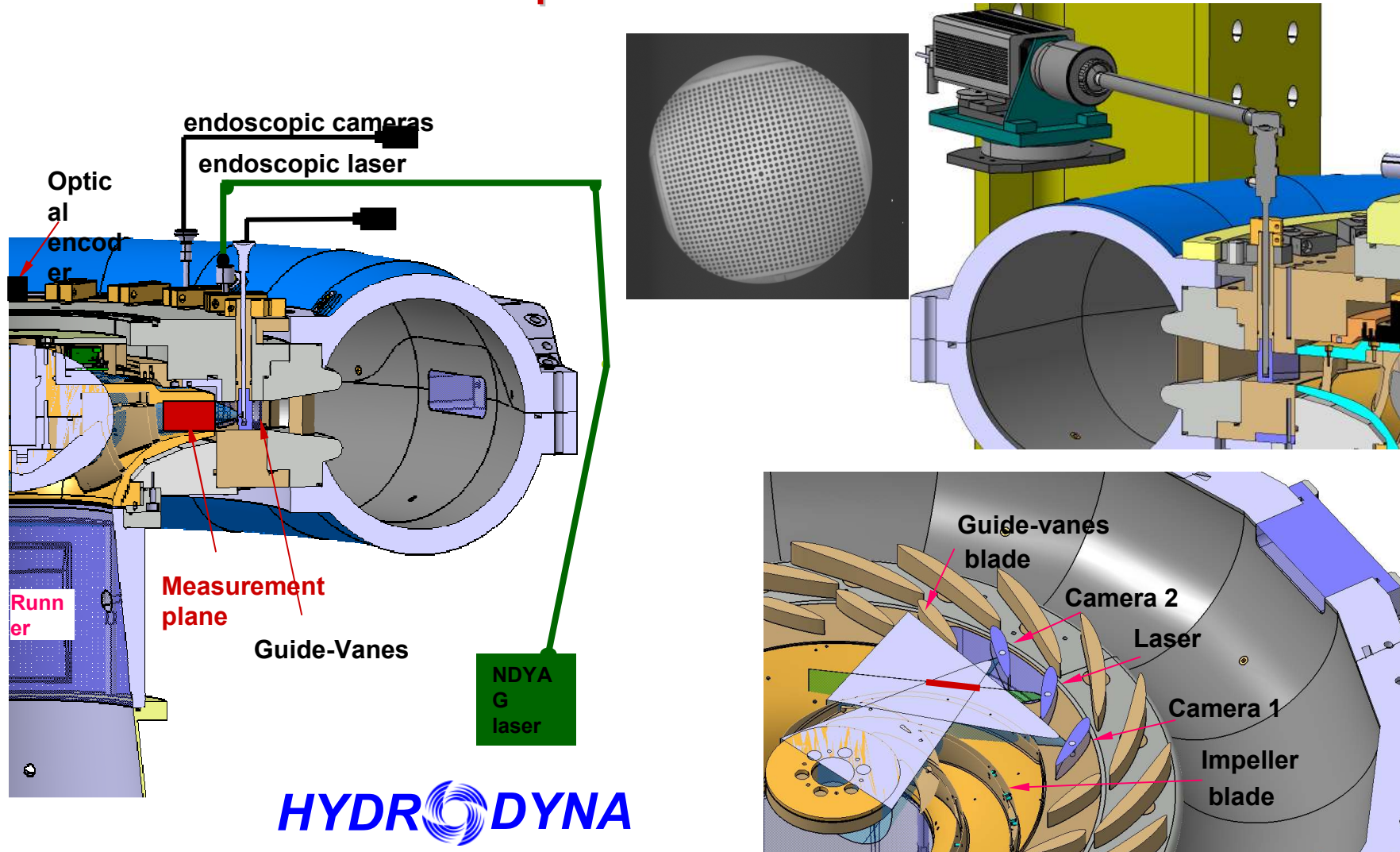
2 Phases PI'

$$\vec{r} = \vec{r}(\theta) = x(\theta)\vec{i} + y(\theta)\vec{j} + z(\theta)\vec{k} \quad \begin{cases} x = r_o b^{\theta/2\pi} \cos \theta \\ y = r_o b^{\theta/2\pi} \sin \theta \\ z = z_o - r_o (b^{\theta/2\pi} - 1) / \tan \beta \end{cases}$$



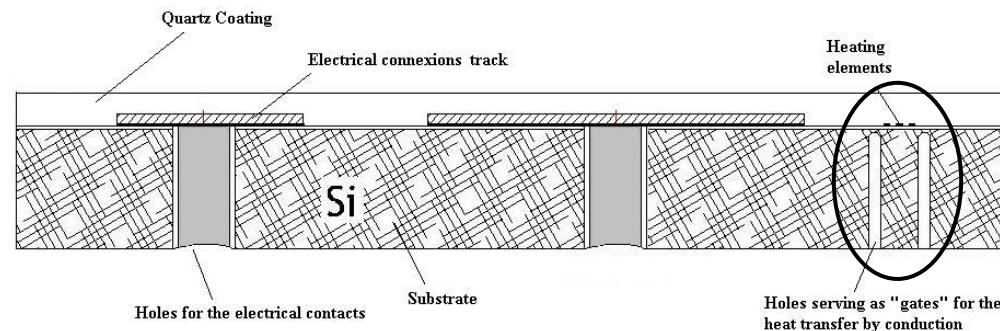
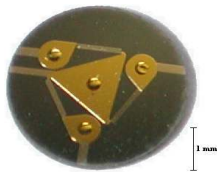
		Cavitation-free vortex	Vapors-core vortex
Initial radius	r_o	0.09	0.15
Initial depth	z_o	-0.615	-1.2
Rate of radial growth	b	3.2	4
Cone angle	β	17°	25.5°

Endoscopic PIV in the Runner



1. Design and Fabrication of the Miniature Probe

SERIE I



Validations:

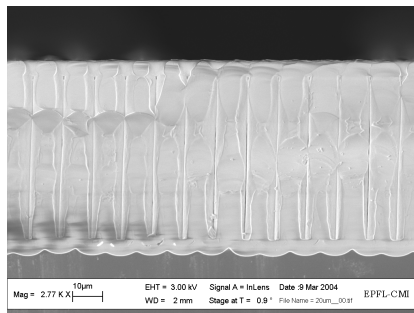
- *Isolation between the surface of the probe, which comes in contact with the water, and the hot-film;*
- *There were chosen the materials for the hot film, the refilling holes.*

Results:

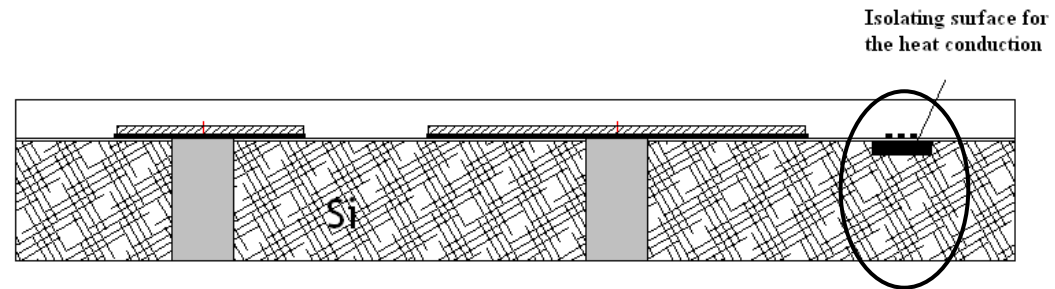
- *a high thermal conduction, even with the gates;*
- *the detachment of the quartz on the electrical connexions;*
- *a very short " life time" in the water (~2-3 days), due to the high thermal conduction*

1. Design and Fabrication of the Miniature Probe

SERIE II



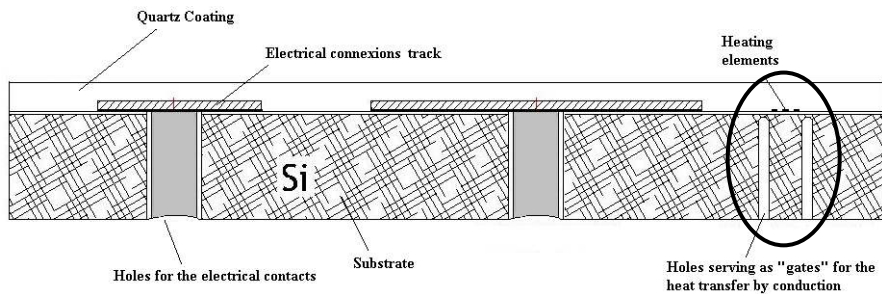
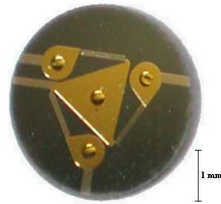
Example of refilled Si pillars performed at CMI



New studied parameters:

- *The thickness of the silicium pillars, for optimizing the refill with the SiO₂ layer.*
- *The optimally forms and dimensions of the pillars in order to realise a compact and solid substrate*

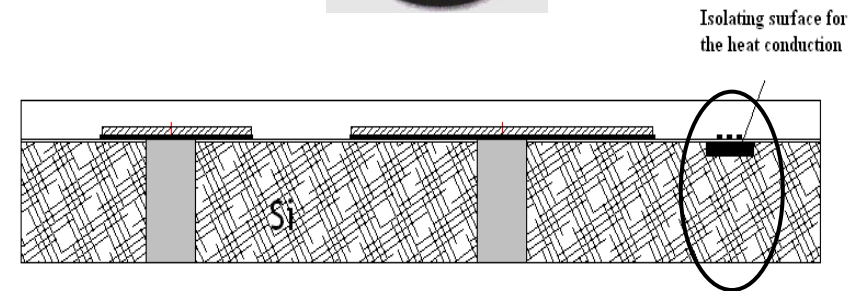
1. Design and Fabrication of the Miniature Probe



Serie I

Results:

- ✓ high thermal conduction;
- ✓ detachment of the quartz on the electrical connexions;
- ✓ very short " life time" in the water (~2-3 days).



Serie II (3
wafers)

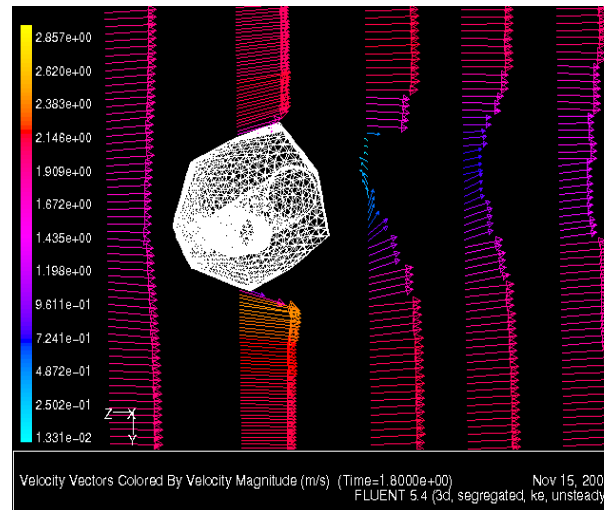
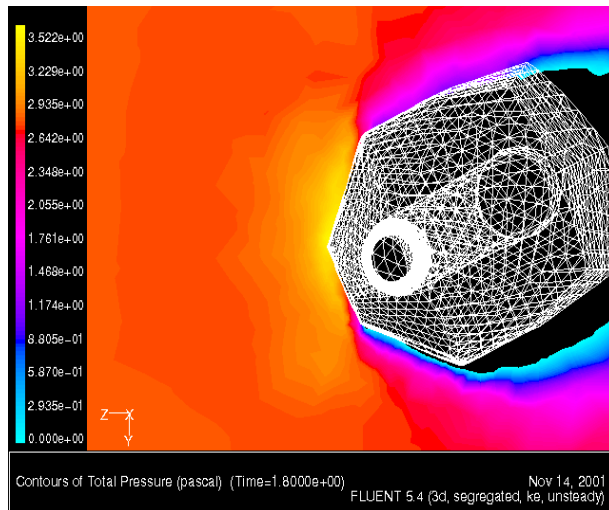
Similarities

- ✓ Hot films, refilling holes, substrate, electrical connexions materials;
- ✓ Design

Differences:

- ✓ Thermal isolation's realisation: gates against isolating surface
- ✓ New studied parameters:
 1. Thickness of the silicium pillars;
 2. Optimally forms and dimensions of the pillars

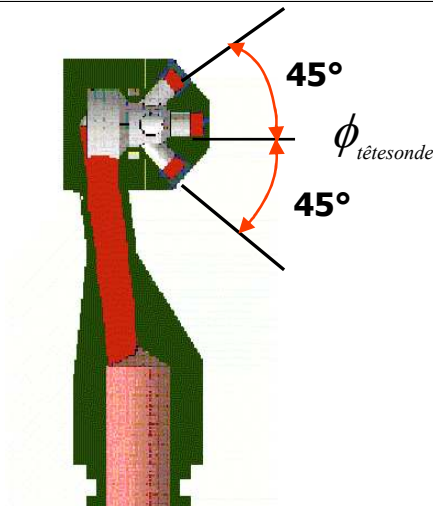
Unsteady Pressure Probes



Probe:

- ✓ angles 90° & 90°
- ✓ diameter 10 mm

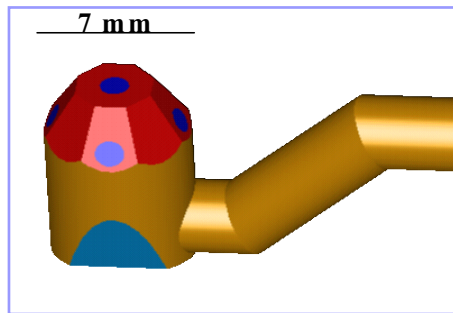
1 calcul $\alpha = 0^\circ$, $\tau = 0^\circ$
2 calcul $\alpha = 25^\circ$, $\tau = 0^\circ$



- ✓ shape of the probe head = pyramid
- ✓ probe opening angle = 90°
- ✓ external diameter of the probe = 9.24 mm
- ✓ sensors: UNISENSOR 0-5 bar, D=2mm, H=1.5 mm

Unsteady Pressure Probes

Unsteady total pressure
probe INPG



Angles : 55° & 55°
Sensitivity: 3 units F / $50^\circ \alpha$
3 units G / $50^\circ \tau$

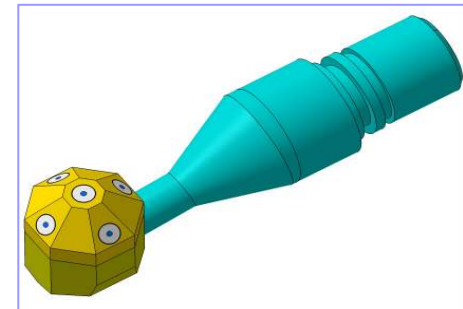
Unsteady total pressure
probe LMH

United Sensor Geometry



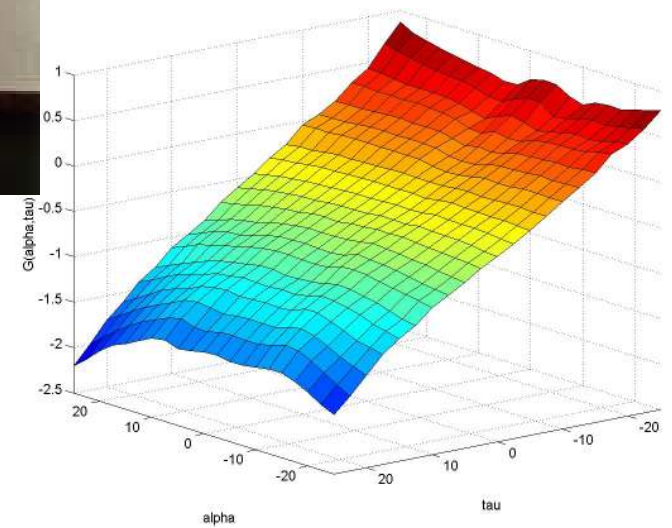
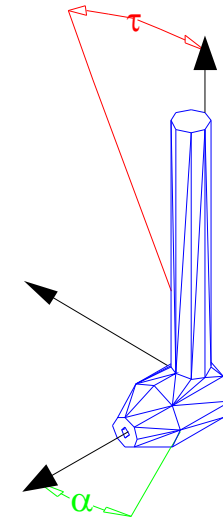
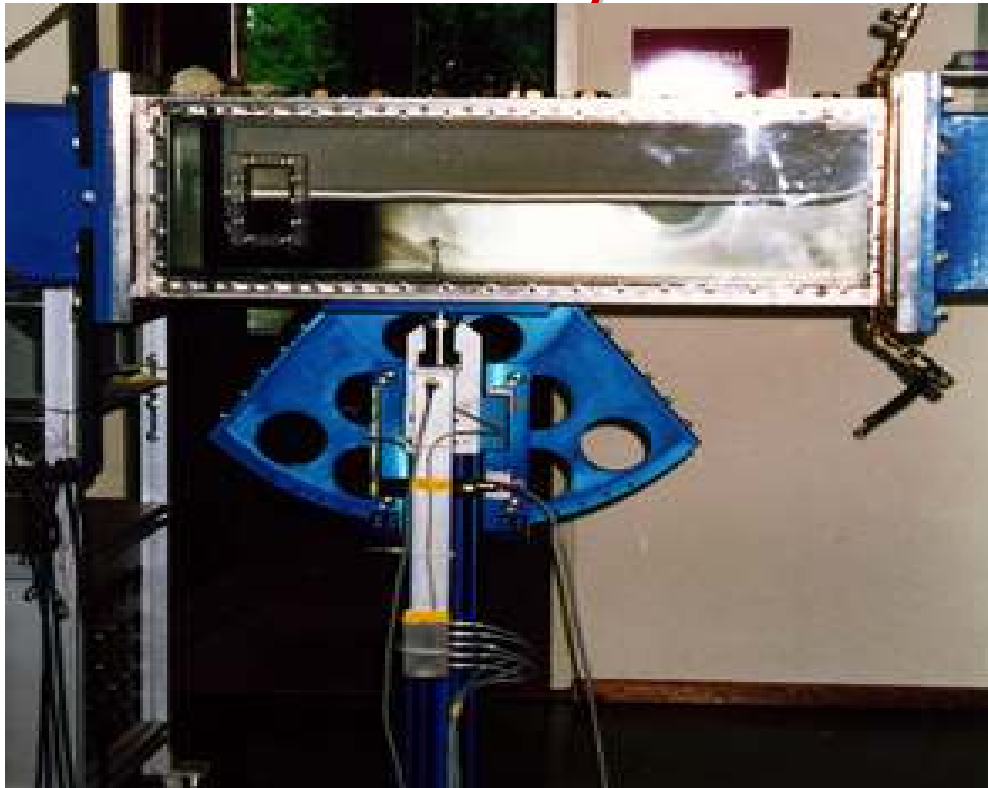
Angles: 100° & -90°
Sensitivity: 8 units F / $50^\circ \alpha$
1.4 units G / $50^\circ \tau$

Unsteady total pressure
probe LMH



Angles: 90° & -90°
Sensitivity: 4 units F / $50^\circ \alpha$
4 units G / $50^\circ \tau$

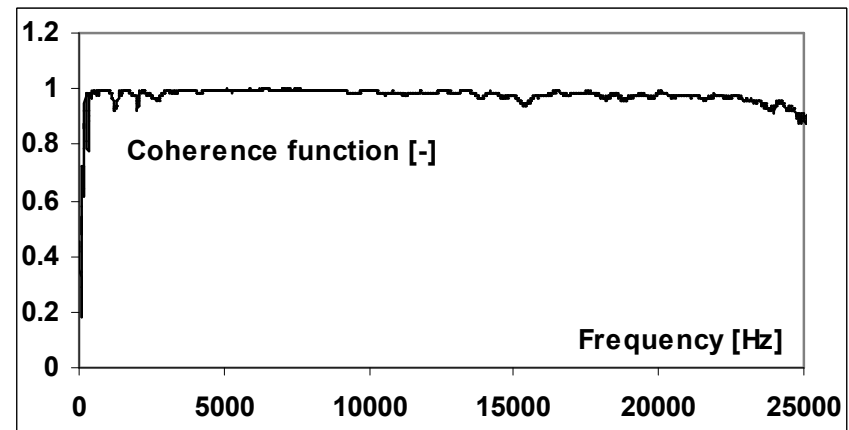
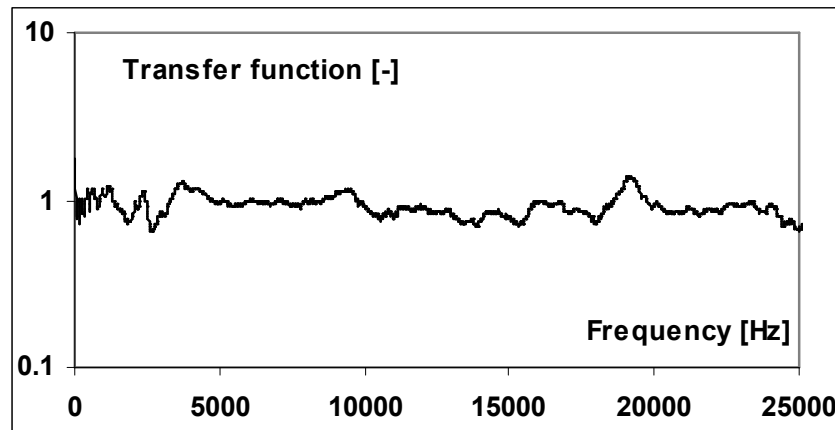
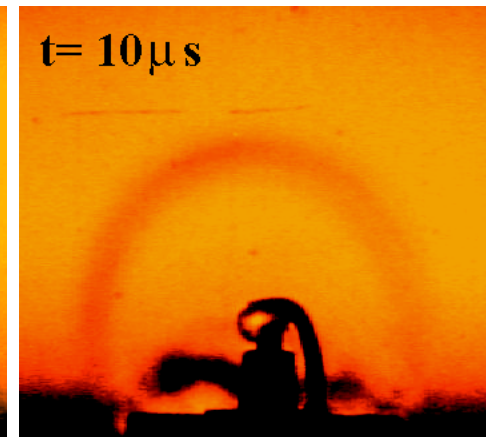
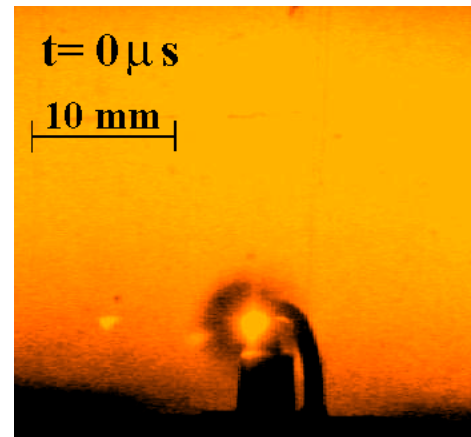
Unsteady Pressure Probe



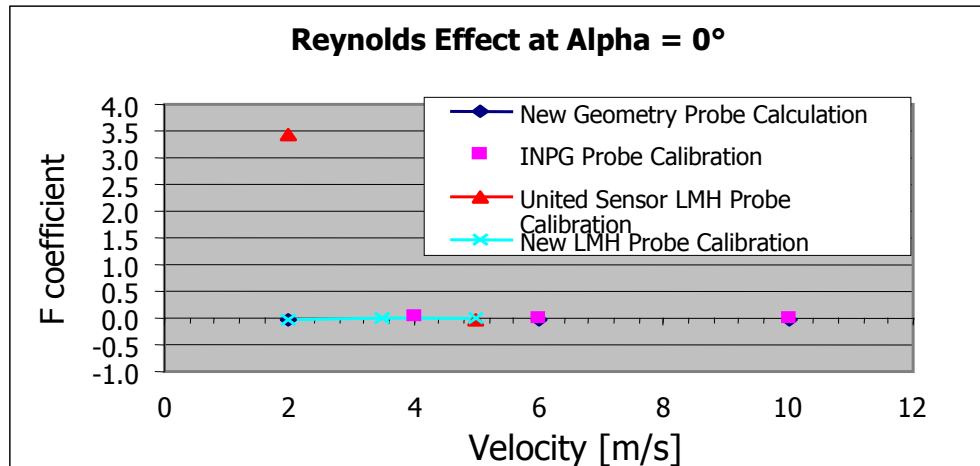
Calibration

Dynamic calibration

- Pressure wave obtained by bubble implosion
- Linear by 25 kHz

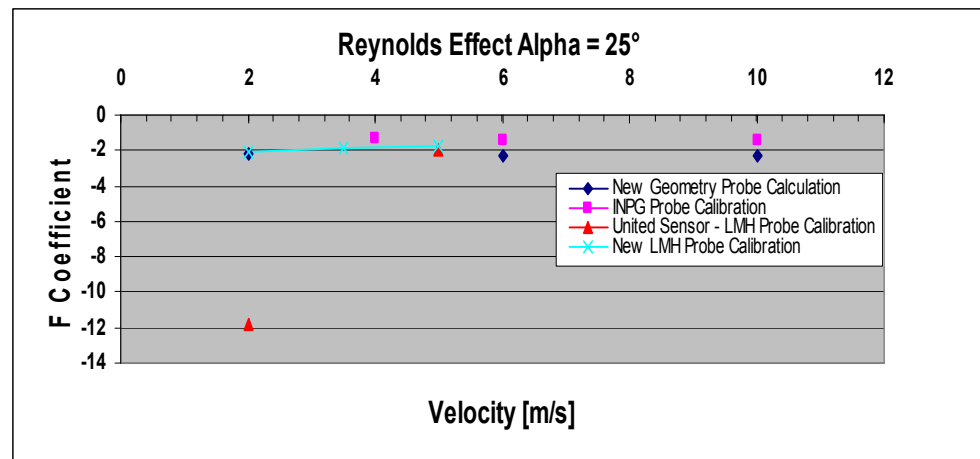


Reynolds Effect



Probe numerical simulation :

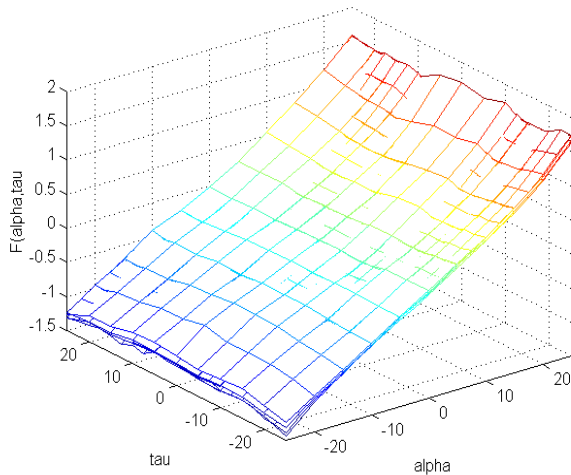
- ✓ *between 2 & 10 m/s*
- ✓ *variation F à 0° = 0%*
- ✓ *variation F à 25° less 4%*



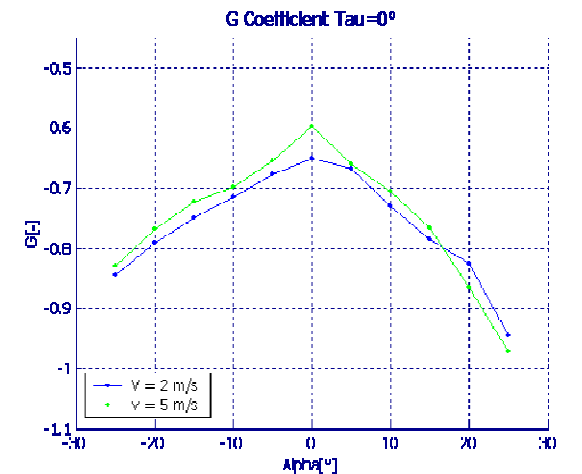
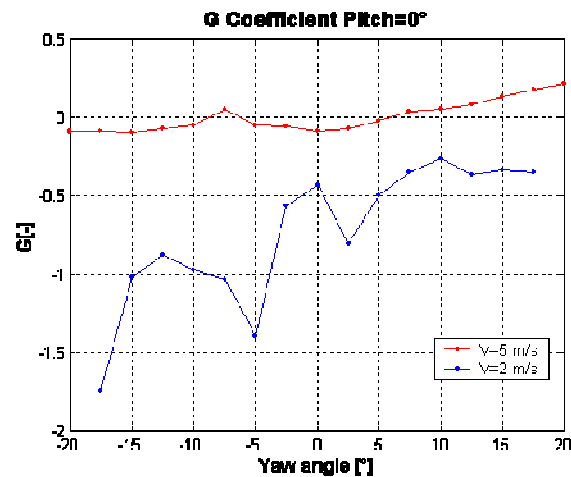
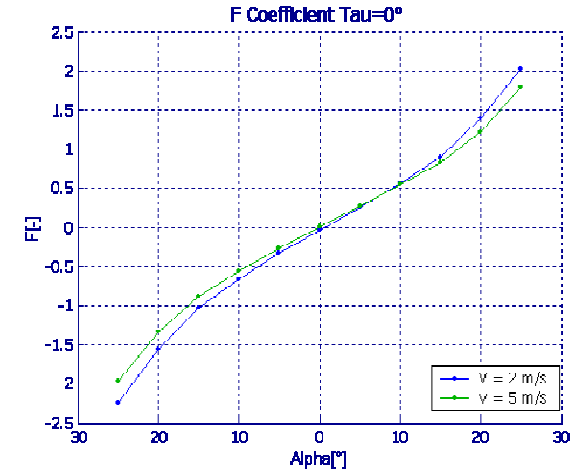
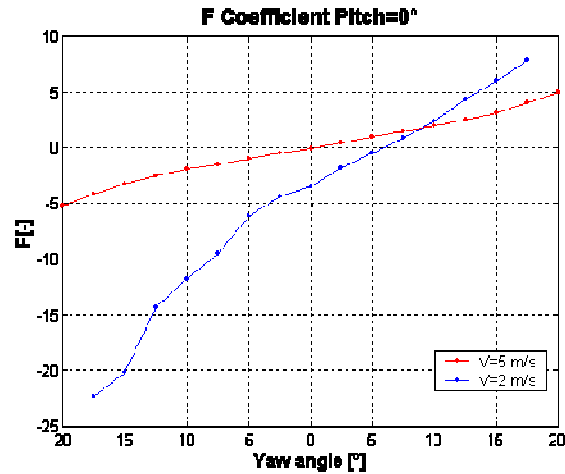
Probes calibration:

- ✓ *between 2 & 5 m/s*
- ✓ *variation F à 0° = 0%*
- ✓ *variation F à 25° less 2%*

Reynolds Effect



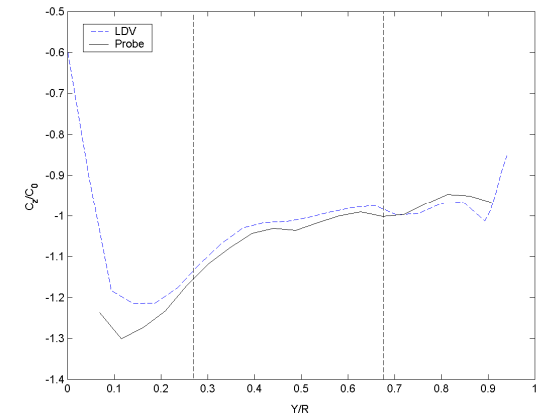
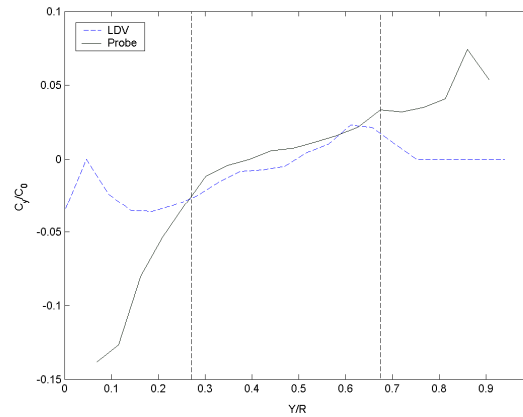
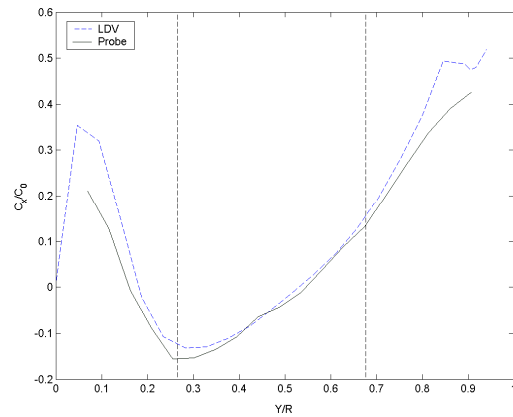
Sonde INPG 4 -10 m/s



Sonde United Sensor - LMH 4 - 8 m/s

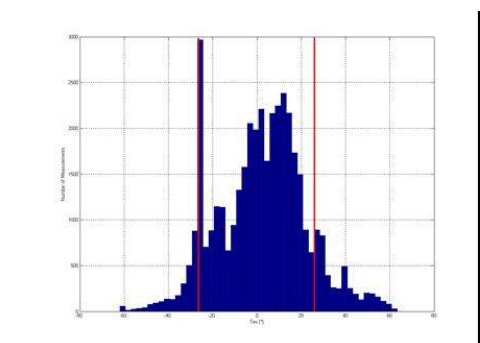
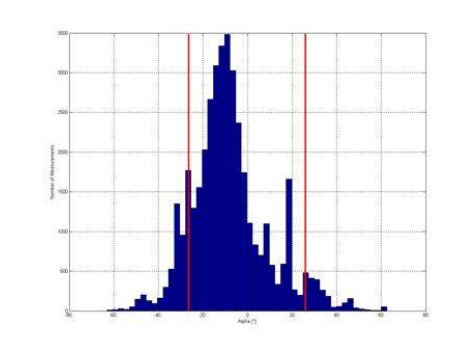
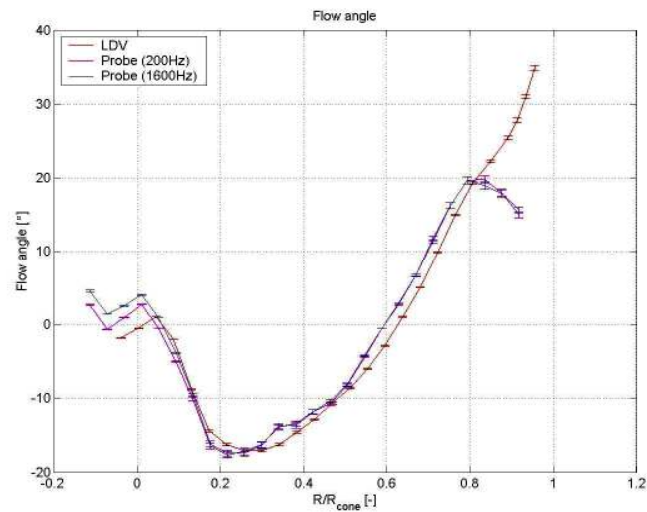
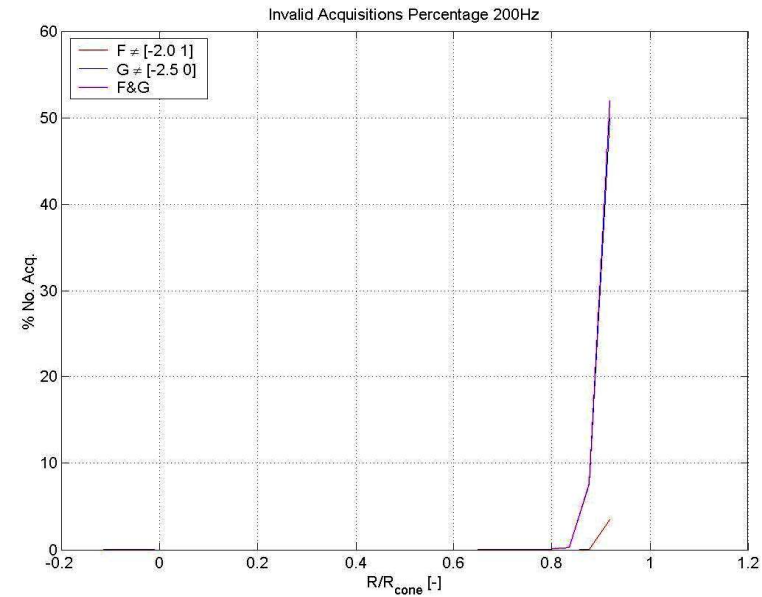
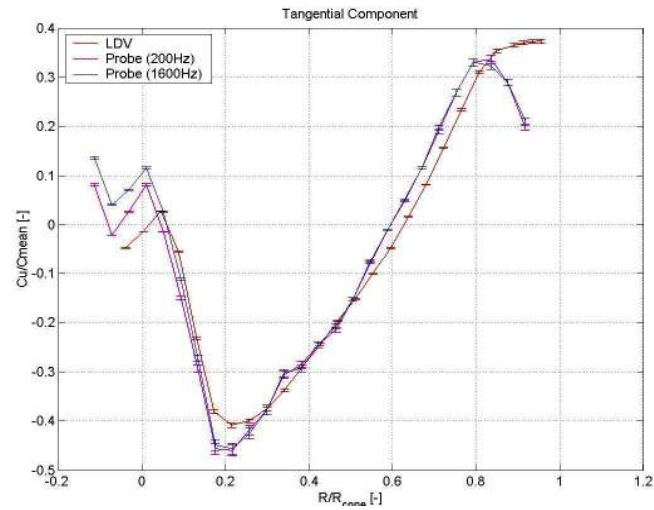
Sonde LMH 2 – (5) m/s

Unsteady pressure measurements



✓ *Validity domain of the probe accuracy*

Unsteady pressure measurements



Conclusion

- ✓ *Strong needs in the hydraulic machinery development:*
 - ✓ *New market needs*
 - ✓ *New developments with strong environmental, exploitation and operation constraints*

- ✓ *Can be insured by:*
 - ✓ *New high accuracy tools development: theoretical, experimental and numerical*
 - ✓ *Multidisciplinary approach to solve new topics*

